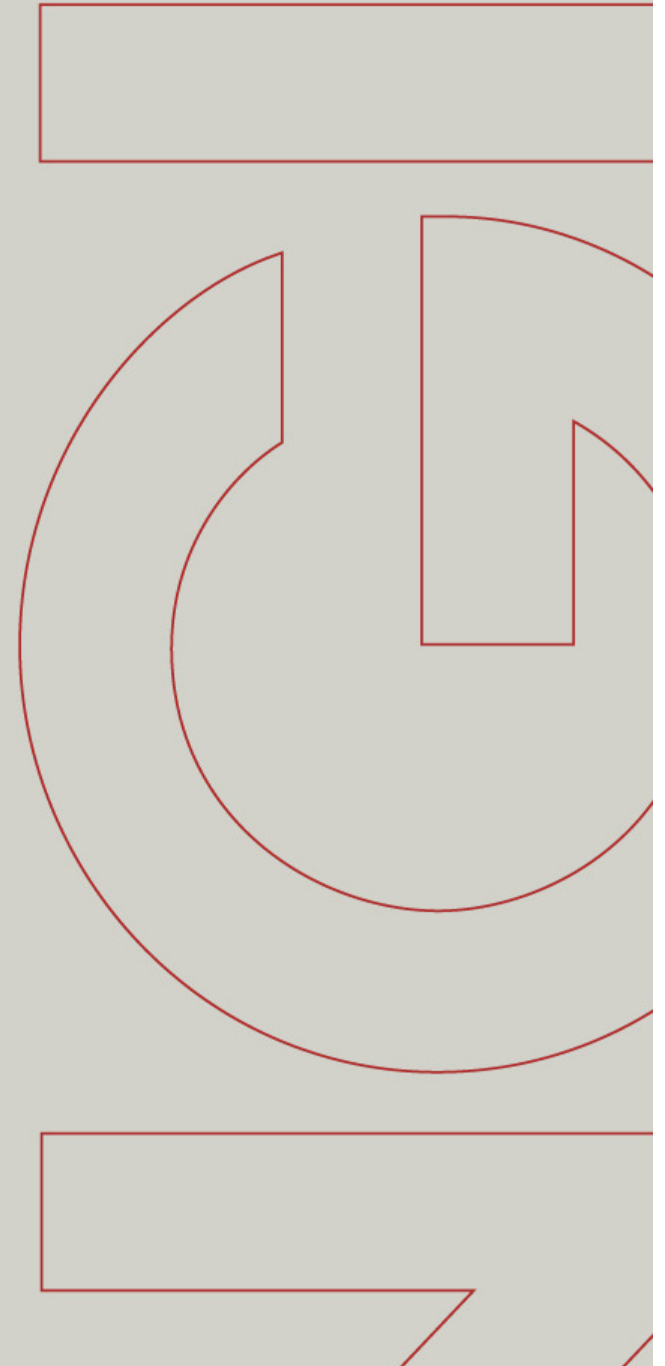


Norwegian Tunnelling Technology  
Workshop in Singapore 17-18 February  
2009

# Support Design and Documentation during Tunnelling

By Eystein Grimstad  
NGI



# Content

- Main principles of the Norwegian tunnelling
- Rock mass classification with the Q-system
- Support design
- Energy absorption and ribs of sprayed concrete
- Documentation during excavation

## **Tunnels in Norway**

- 700 railway tunnels

Total 285 km railway tunnels

Longest railway tunnel 14,5 km

- 914 road tunnels

Total 802 km road tunnels + twin tube

Longest road tunnel 24,5 km

(longest in the world)

- About 4000km of hydropower tunnels. More than 200 underground power houses

NING

# NMT- Norwegian Method of Tunnelling

## Norwegian Tunnelling Technology

- Mainly in hard rock ( $\sigma_c = 3-300$  MPa)
- Mainly drill and blast, but also TBM
- Rock Mass Classification with the Q-system
- Rock support mainly Sfr + B and RRS
- Temporary support forms part of permanent support
- Design as you go based on the Q-system++
- Drained solutions. Pregrouting in built up areas and subsea
- Sfr single shell as final lining + B for rock support
- Water shielding and frost protection
- Ventilation, illumination, security installations



# NMT-principles

Difference between NATM and NMT

## NMT

- Most appropriate for hard rock
- Temporary support based on rock mass classification (Q-system ++)
- Monitoring when deformation is expected
- Fibre reinforced sprayed concrete + rock bolts +RRS as temporary and permanent support
- Temporary support+supplement and water shielding act as permanent support
- Drainage +ventilation+illumination
- **Cost 4,000 -9.000 Euro/m tunnel**

## NATM

- Most appropriate for soft ground
- Temporary support based on 5 or 6 classes (deformation and hardness)
- Monitoring of deformation
- Steel sets +lattice girders + sprayed concrete as temporary support
- Permanent support is pre designed
- Watertight membrane
- Cast concrete lining including the invert as final support
- Ventilation+illumination
- **Cost 21.000-50.000 Euro/m tunnel**

# Basis for decision of rock support

- The rock should be a part of the construction
- Various background experience (tomb rules, practice etc.)
- Systematic rock mass classification
- Numerical analysis
- Geological conditions
- Variation in stability
- Various application of the underground structure
- Required level of safety and durability












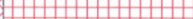
# Preinvestigations with Q-system

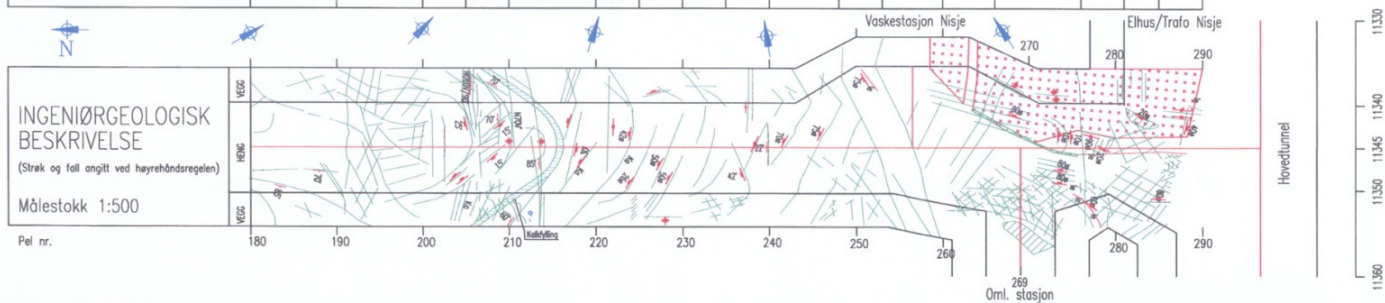
- Some of the parameters may be uncertain in the terrain, but will give a good tool for rock mass classification
- RQD,  $J_n$  og  $J_r$  are normally reliable in the terrain
- Joint frequency and weathering increase towards the surface
- $J_a$  and  $J_w$  are often difficult to map in the terrain ( $J_a$  OK in fresh rock cuttings)
- SRF has to be estimated from topography, overburden and knowledge about rock stress in the area. Stress measurements may be performed.
- Q-values, (also  $J_w$  from water loss tests) from core logging

# Rock mass classification in tunnels






- Mapping before spraying of concrete
- Has to be done from a platform or basket close to the crown and face
- General geological mapping– rock types, structures, joint geometry, orientation of weakness zones, width, mineral filling etc.
- Map sections of the tunnel with uniform Q-values if many rounds are available at the same time before spraying
- Large single blocks, long joints parallel to the tunnel etc., has to be evaluated in addition to the general rock mass classification

## Tunnel map with Q-values and support classes

Merknad	Leirskifer														Leirskifer/hornfels				Leirskifer/knollekalk og porfyrisk Syenitt							
Klassifisering/bergart	Leirskifer					Leirskifer/hornfels				Leirskifer/knollekalk og porfyrisk Syenitt																
RQD/Jn	65/9	68/9	75/9	65/9	65/9	85/6	85/6	80/6	75/6	70/6	50/12	50/9	30/15	50/9												
Jr/Ja	2/2	2/2	2/2	2/2	2/2	2/2	1,5/2	2/2	2/2	1,5/3	1,5/3	1,5/4	2/3	1,5/3												
Jw/SRF	1/1	1/1	1/1	1/1	1/1	1/1	1/1	1/1	1/1	1/1	1/1	0,7/1	1/1	0,7/1												
Q – verdi	7	11	12,5	6-8	7	14	11	13	12	6	2	1,8	1,3	1,8												
PERMANENT-SIKRINGSKLASSE	C		B		C			B				C		D												
																										
																										
Pei nr.	180	190	200	210	220	230	240	250	260	270	280	290														







[illegible]TEGNFORKLARING

	Lagdelling/skifrighet uten leire
	Lagdelling/skifrighet med leire
	Horisontal/vertikal orientering for lagdelling, skifrighet
	Sprekk uten leire
	Sprekk med leire
	Horisontal/vertikal orientering av sprekk


 Leir-/knusningsone  

 Tett, parallell oppsprekking  

 Intrusivgang  

 Foldeakse  

 Bergartsgrense

kv - kvarts  
le - leire  
kl - kloritt  
sv - svelleleire  
ka - kalkspat

FJELLSIKRINGSKLASSER

	KLASSE A = $Q > 40$
	KLASSE B = $10 < Q < 40$
	KLASSE C = $4 < Q < 10$
	KLASSE D = $1 < Q < 4$
	KLASSE E = $0,1 < Q < 1$
	KLASSE F = $Q < 0,1$

000	Som byggelst	10.03.2008	XERMA	Per & Møen	KJ&Sten
Rev.	Revisjonen gjelder	Dato	Tegnet av	Arbeidet av	Gjeldet av
ASKERBANEN, BIERUMTUNNELN Tverslagstunnel Km: 0,180-0,290 Ingeniørgеologisk kartlegging			Format:		
			Målestokk:	Tvers tunnel: 1:500	
			Målestokk:	Lengde tunnel: 1:500	
			Prosjekt	Jernbaneverket utbygging	
Prod.tegn. av			Erfaringsf. for		
Erfaringsf. for			Erfaringsf. for		
Prosjekt: Storslo Parsell: 54, Fossveien			Tegningsnummer: USA54-6-T-V90002-000		Rev.: 000
 <b>Jernbaneverket</b>			Tegningsnummer:		Rev.:
			UB.108836-000		000



# Estimation of Q-values from drill cores

RQD

J<sub>n</sub> (longitudinal joints under-representative)

J<sub>r</sub>

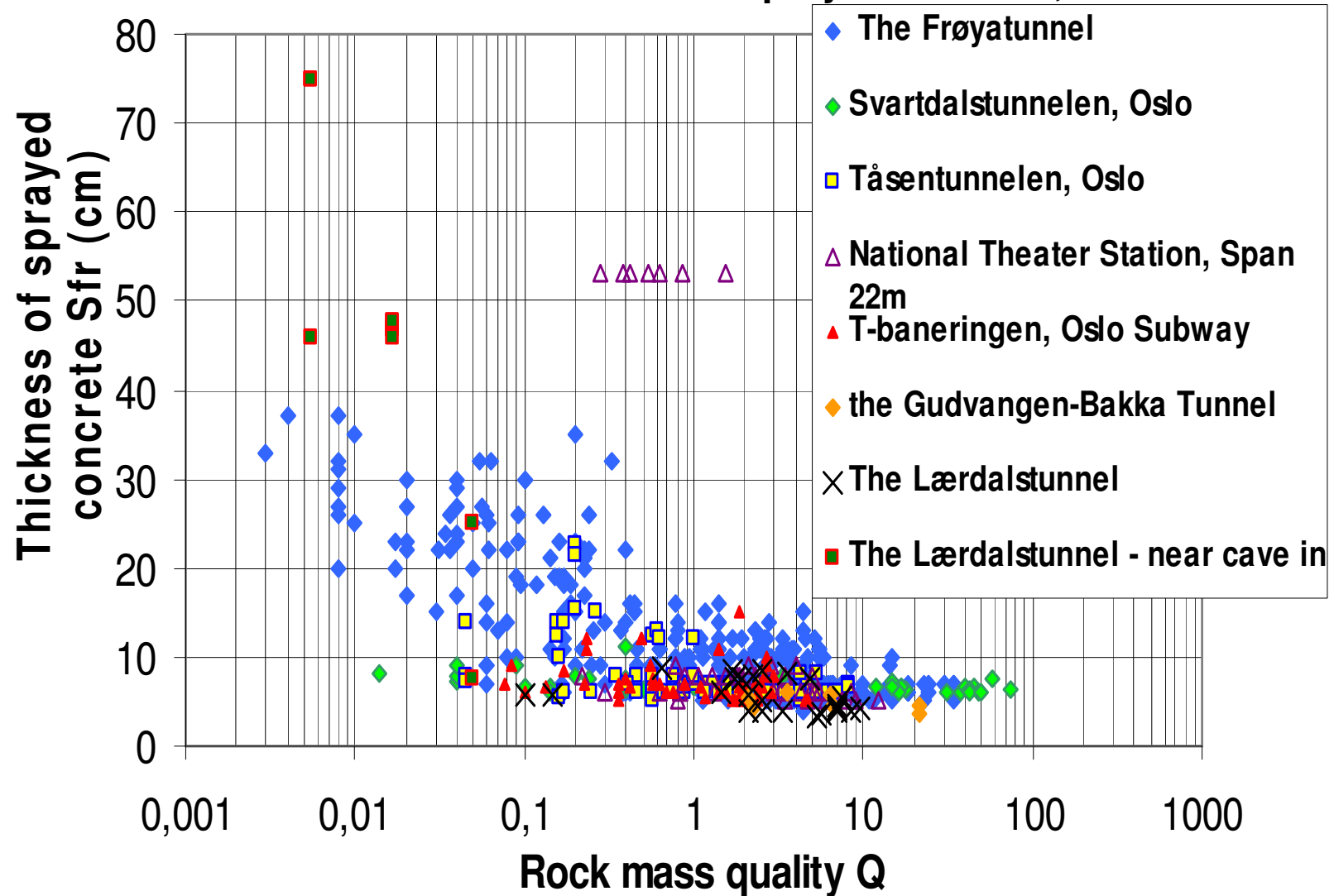
J<sub>a</sub>

Joint frequency

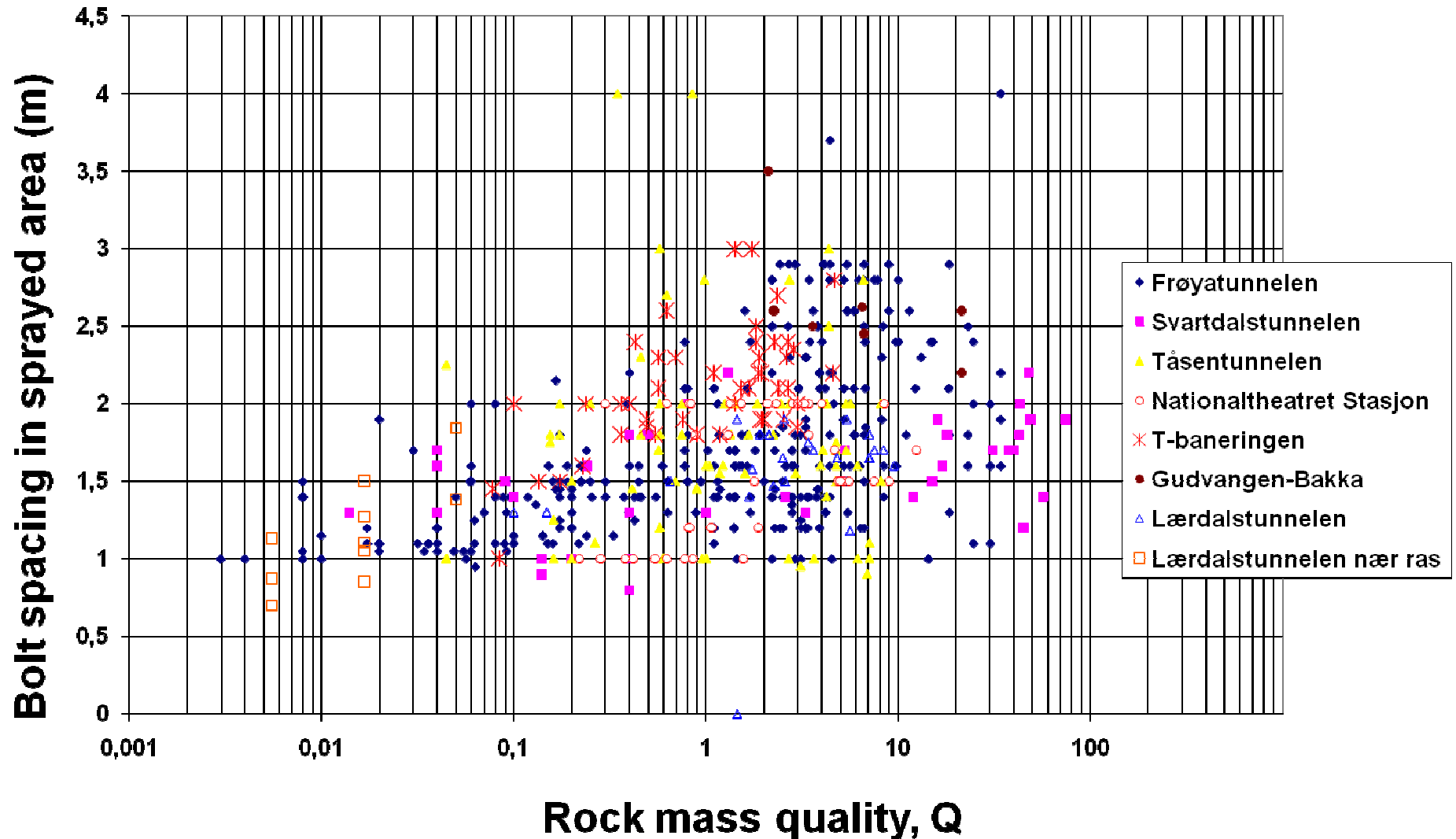


# Thickness of Sfr related to Q

Thickness of fiber reinforced sprayed concrete, Sfr



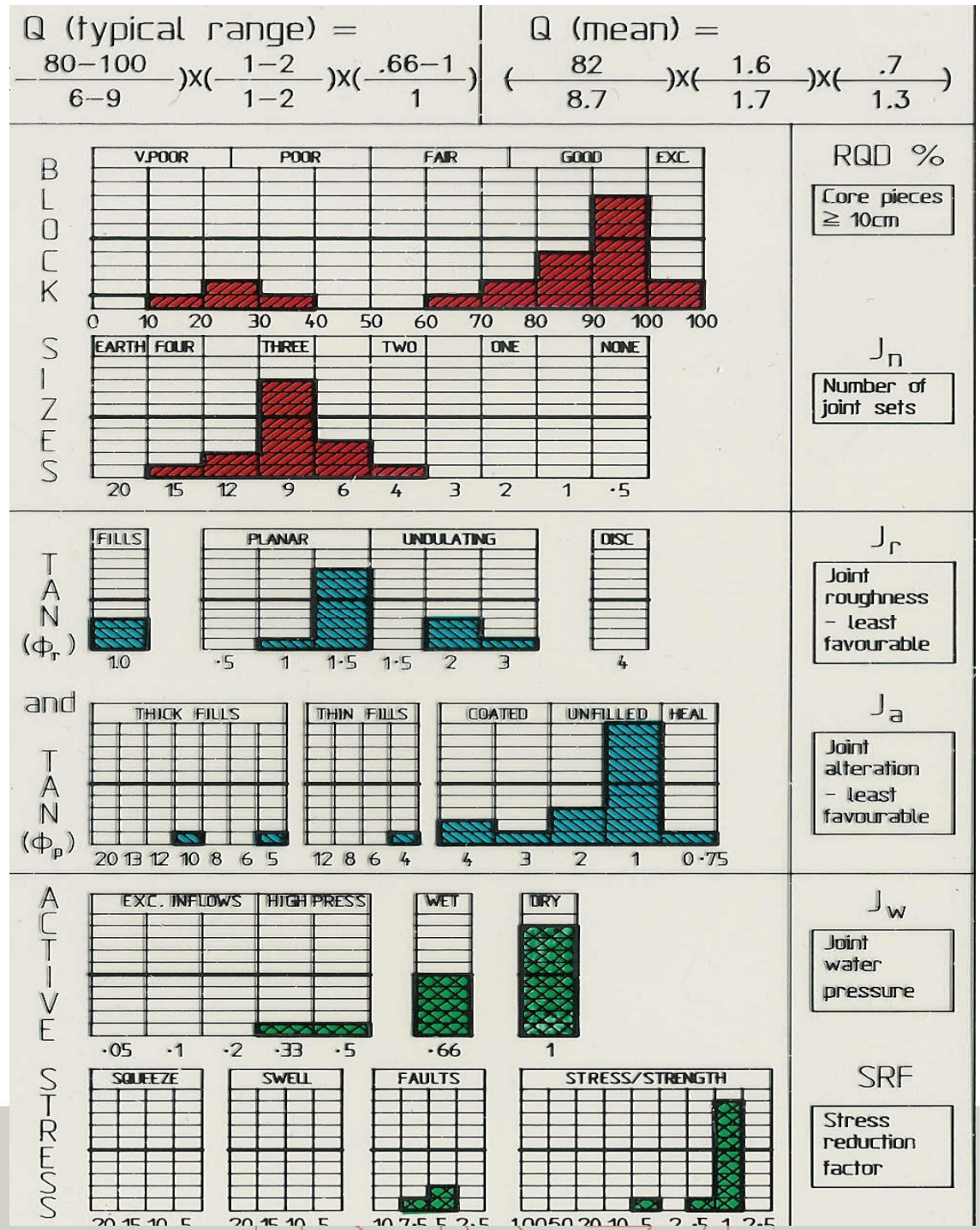
# Bolt spacing in area with sprayed concrete

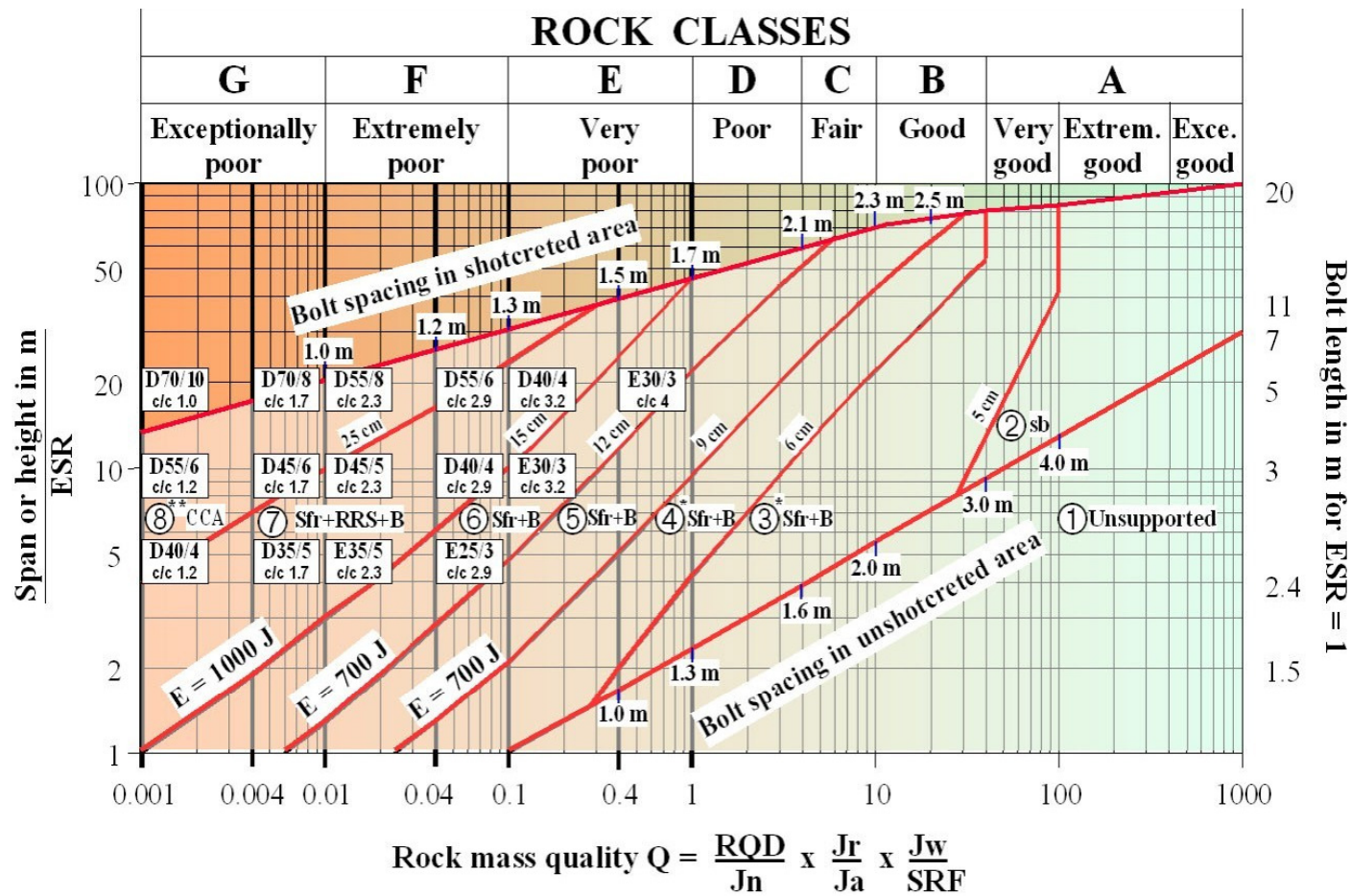




Registration of parameters in histograms gives a good overview for much data.

Spreadsheet gives Max., Min., Average and Typical Q-values for most frequent parameters





#### REINFORCEMENT CATEGORIES

- 1) Unsupported
- 2) Spot bolting, **sb**
- 3) Systematic bolting,  
(and unreinforced shotcrete, 5-6 cm), **B(+S)**
- 4) Fibre reinforced shotcrete and bolting, 6-9 cm, **Sfr+B**
- 5) Fibre reinforced shotcrete and bolting, 9-12 cm, **Sfr+B**
- 6) Fibre reinforced shotcrete and bolting, 12-15 cm, **Sfr+B**
- 7) Fibre reinforced shotcrete > 15 cm +  
reinforced ribs of shotcrete and bolting, **Sfr+RRS+B**
- 8) Cast concrete lining, **CCA** or **Sfr+RRS+B**

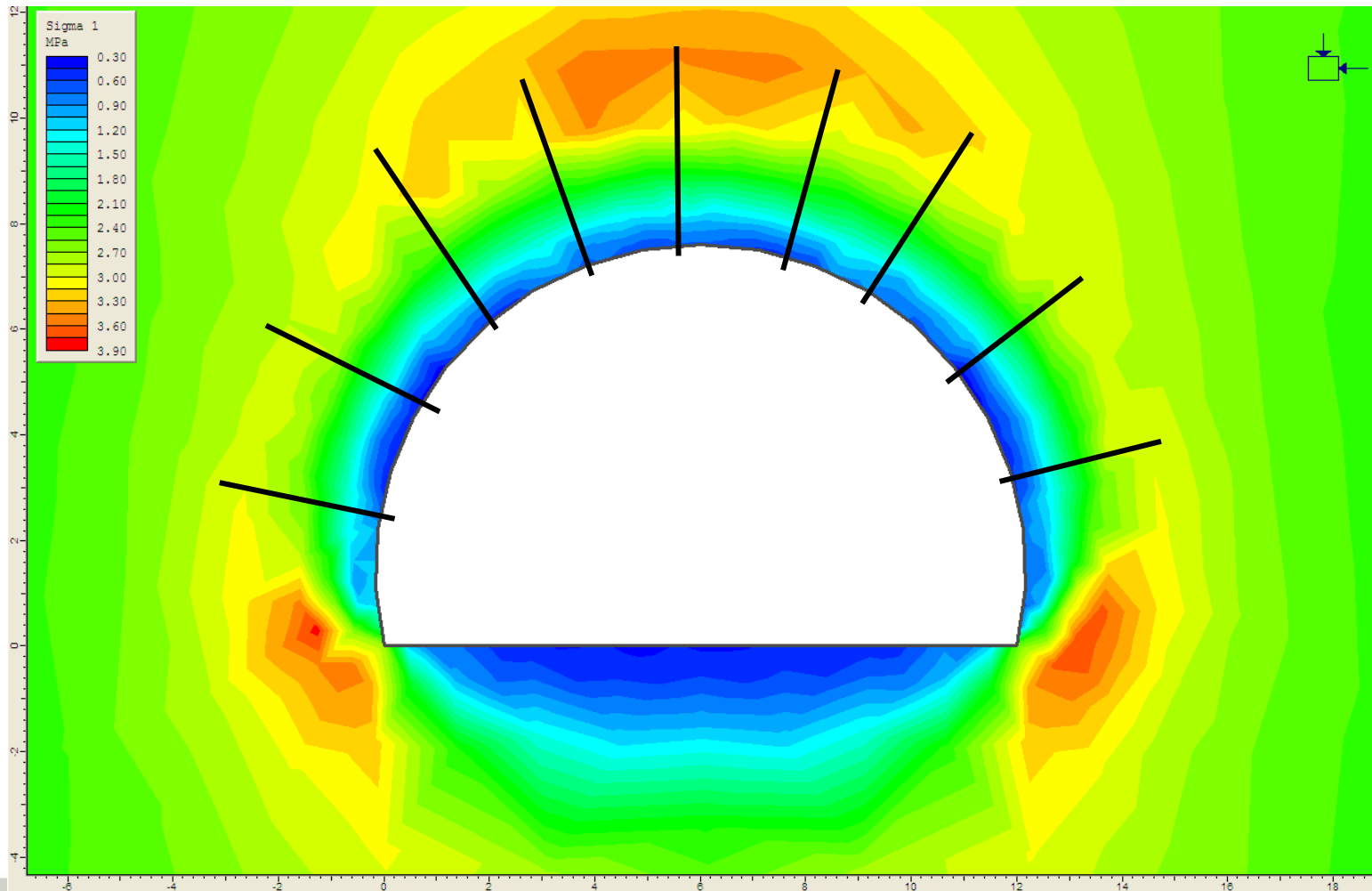
E) Energy absorption in fibre reinforced shotcrete at 25 mm bending during plate testing

**D45/6**  
c/c 1.7 = RRS with 6 reinforcement bars in double layer in 45 cm thick ribs with centre to centre (c/c) spacing 1.7 m. Each box corresponds to Q-values on the left hand side of the box. (See text for explanation)

\*) Up to 10 cm in large spans

\*\*) Or **Sfr+RRS+B**

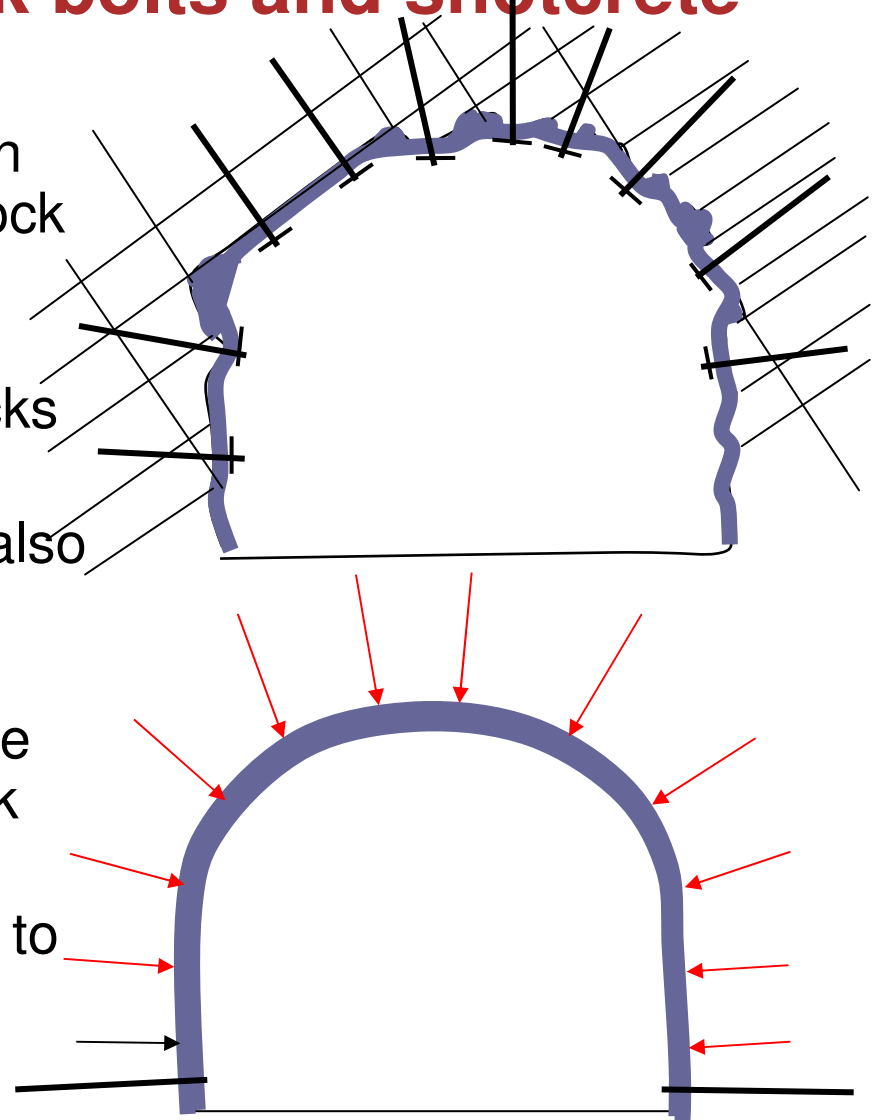
**The rock is also a part of the construction when the rock bolts transfer the forces up to the stable arch**





# Interaction between rock bolts and shotcrete

- Thin layers of shotcrete is a skin taking care of small pieces of rock at the tunnel periphery
- Rock bolts take care of large wedges and prevent larger blocks from falling
- Thick layers of shotcrete need also rock bolts if the periphery is uneven
- Only an even arch may carry the load from poor rock without rock bolts
- Rock bolts always transfer load to the rock



## Rebar end-anchored bolt

- The bolt is pretensioned
- Works after a few minutes
- The Resin anchored bolt is developed especially for installation during excavation
- Excellent in high stresses, also as permanent support



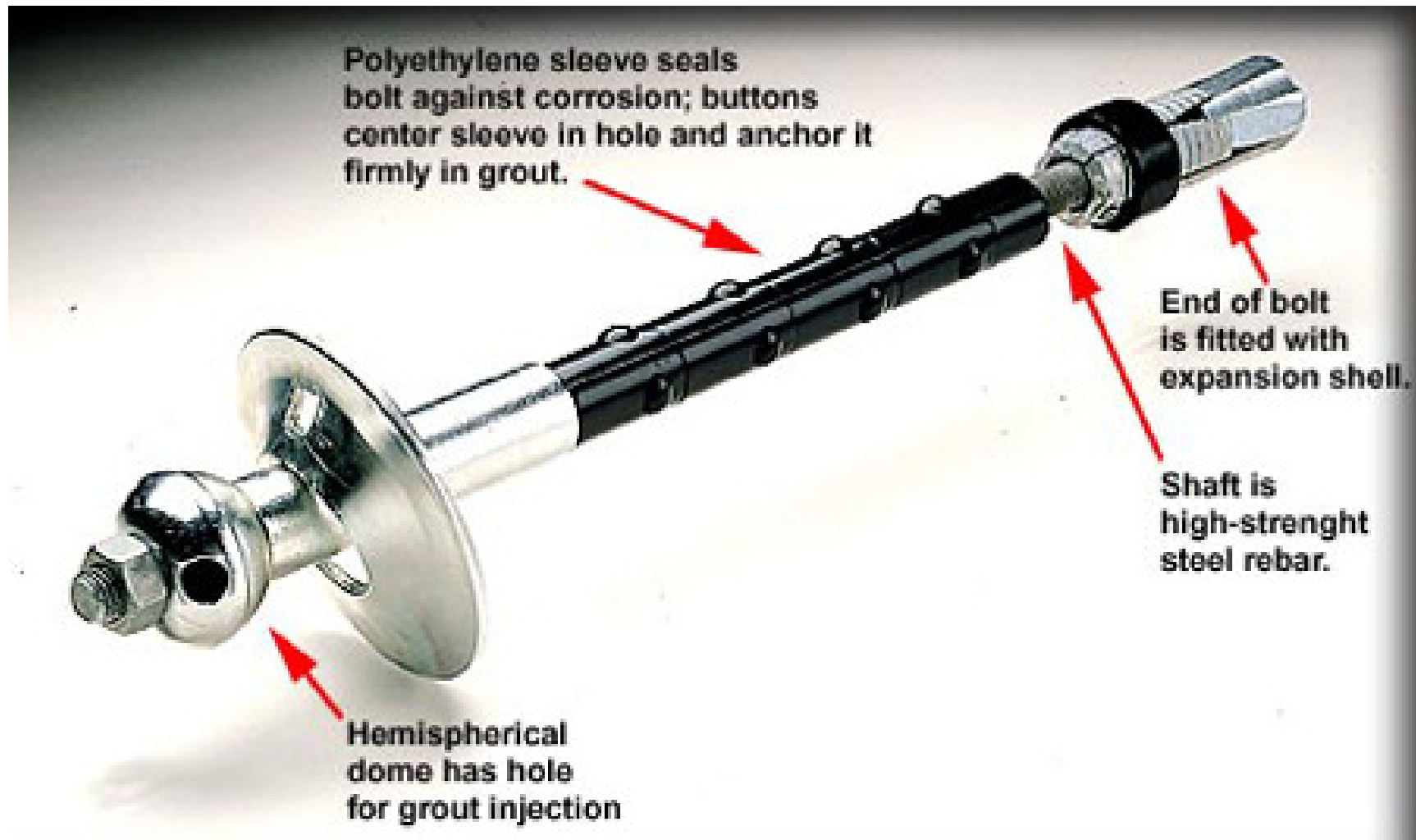
## Rebar bolt for grouting

- The bolt is fully grouted but not tensioned
- Works after many hours
- Suitable for permanent support



## The CT-bolt      5 x corrosion protected

### Combined temporary and permanent bolt

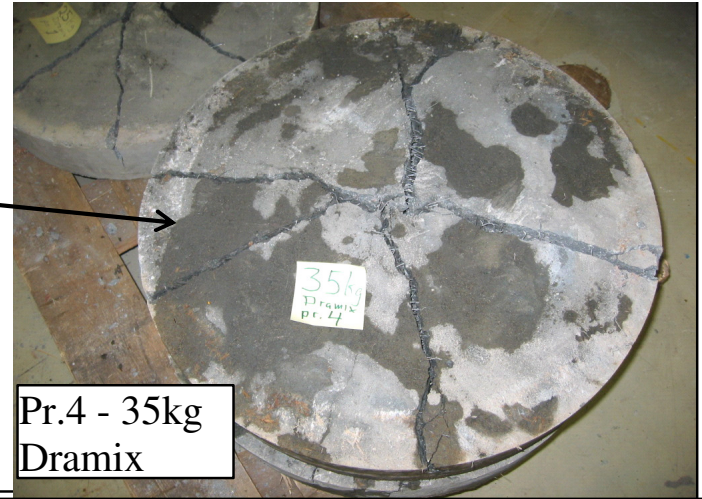


# Testing of energy absorption in sprayed concrete

Some panels were pressed further from 25 to 40mm deflection.



35 kg Dramix  
RC65/35BN steel  
fiber /m<sup>3</sup>

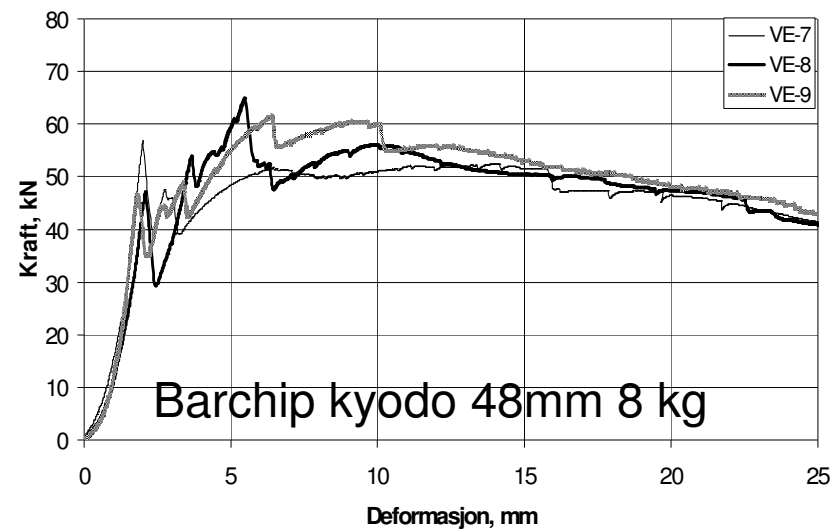
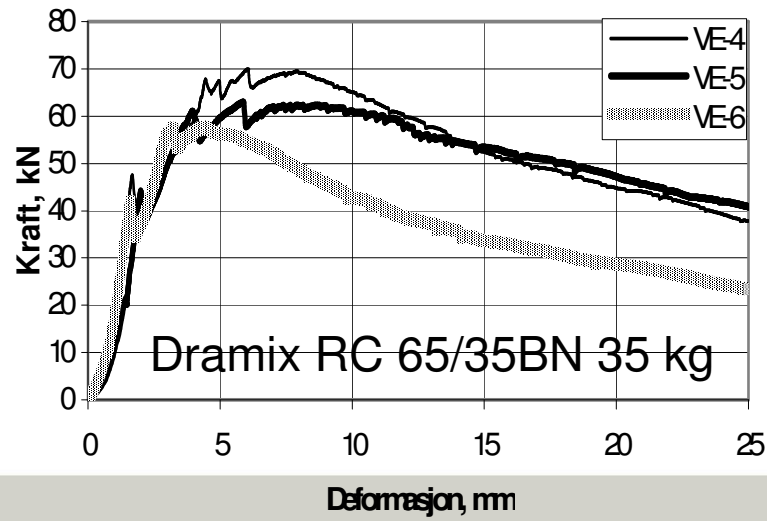
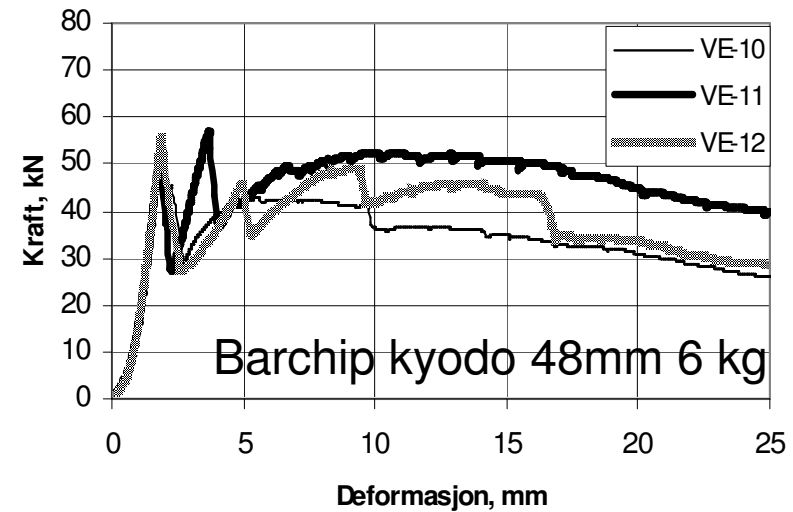
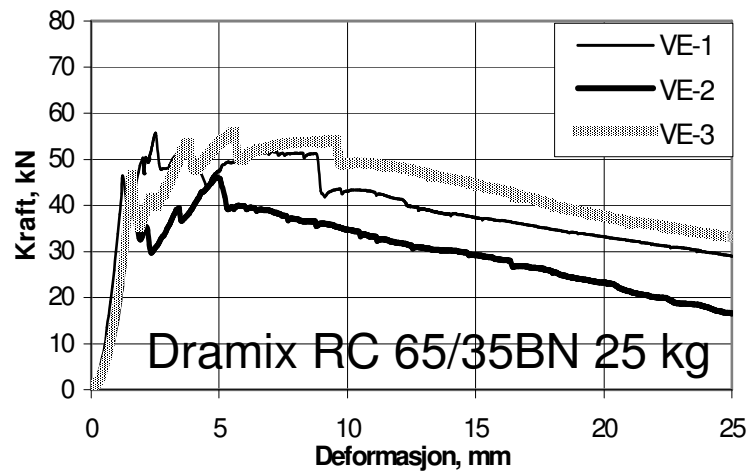


Panel with 7kg  
Barchip fiber after  
40 mm deflection.

8 kg 48mm  
Barchip/m<sup>3</sup>

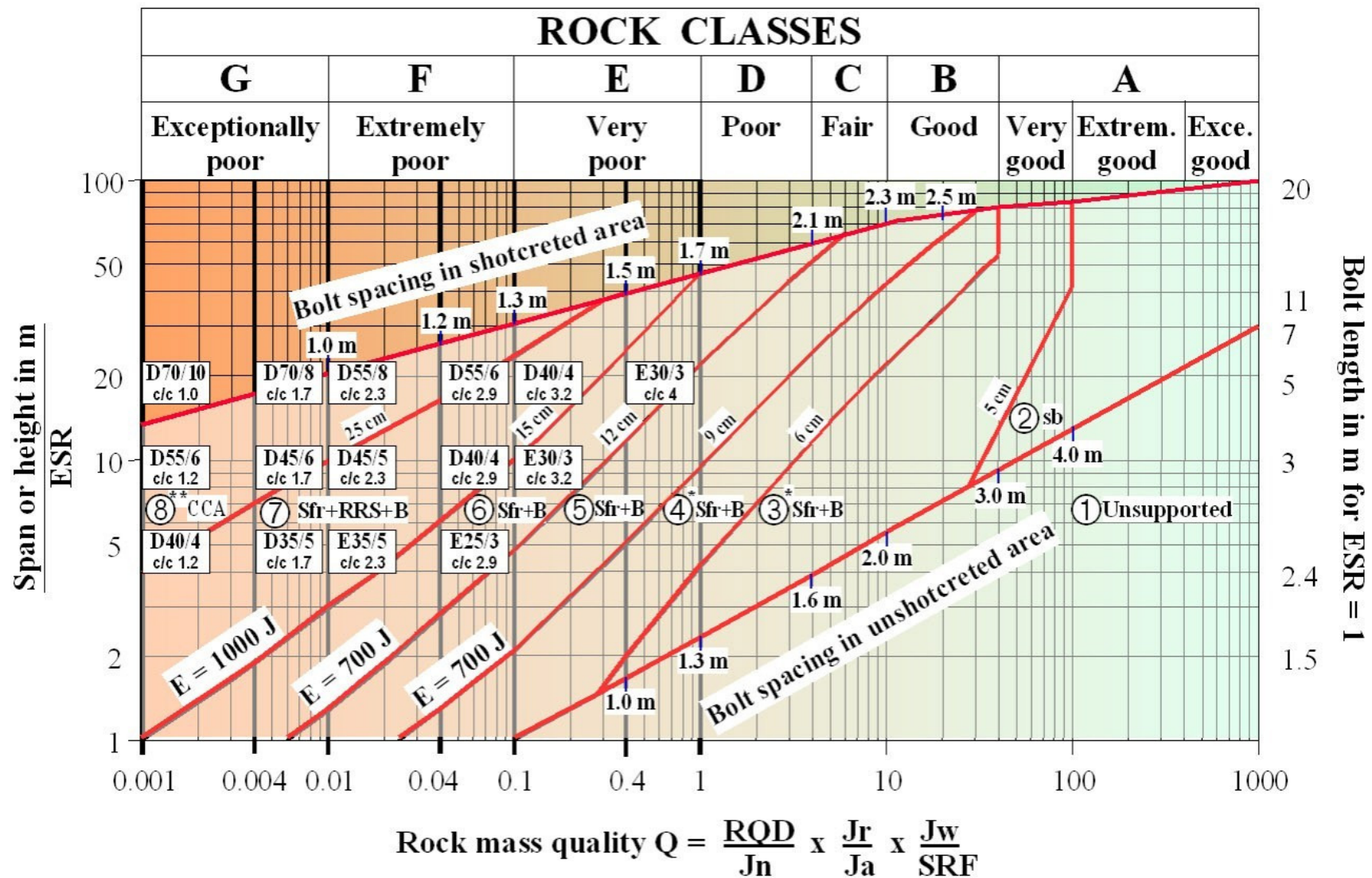


# Comparision between load/deformation curves for panels with Dramix steel fiber and Barchip-composite fiber





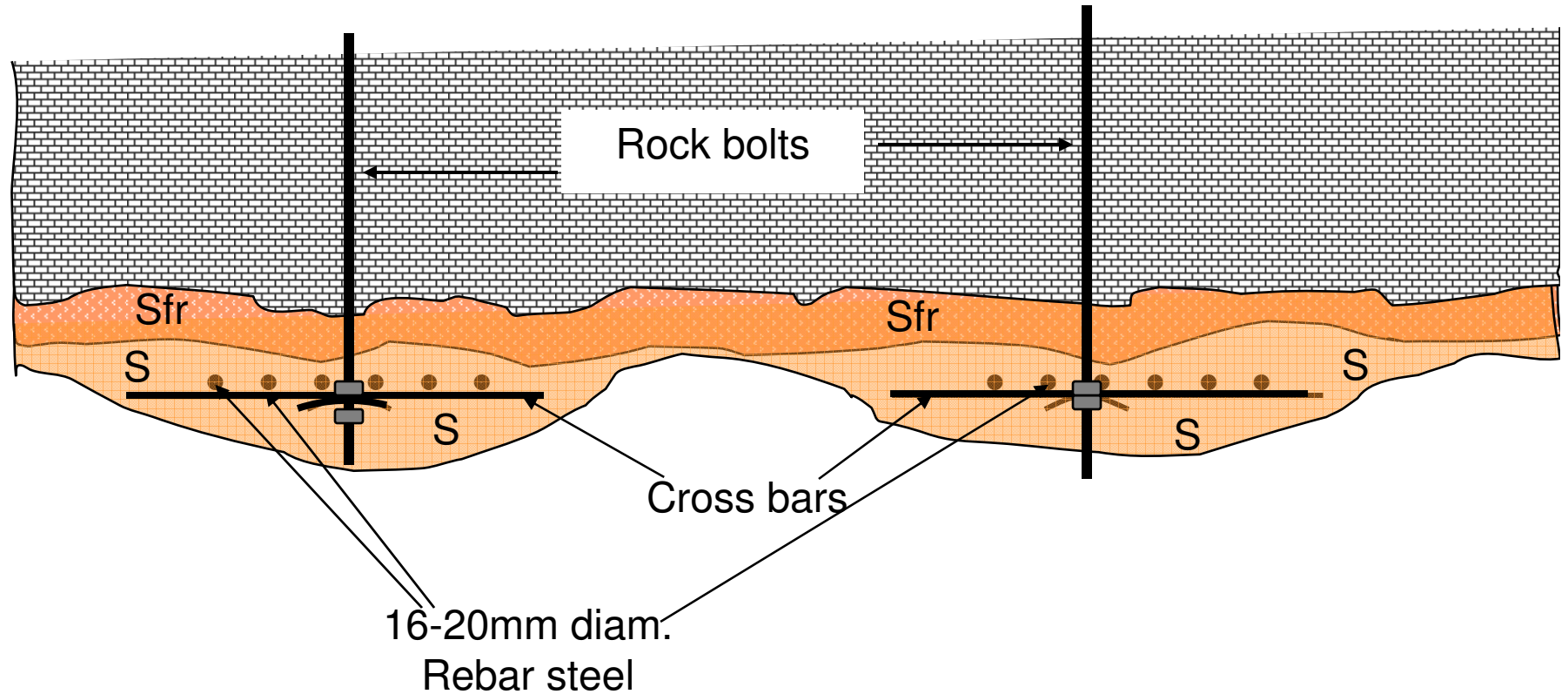
# Energy absorption classes E500, E700 and E1000



# Energy absorption classes

- E500 15-18kg steel fibre or 5kg PP fibre
- E700 20-25kg steel fibre or 6-7kg PP fibre
- E1000 30-35kg steel fibre or 8kg PP fibre
- The Norwegian Road Authority require minimum 8cm thickness of sprayed concrete from the year 2008
- Higher energy absorption classes than recommended by the Q-system
- The Norwegian Road Authority increases the factor of safety in all rock classes

## Cross section of two sprayed ribs



## REINFORCED RIBS OF SPRAYED CONCRETE

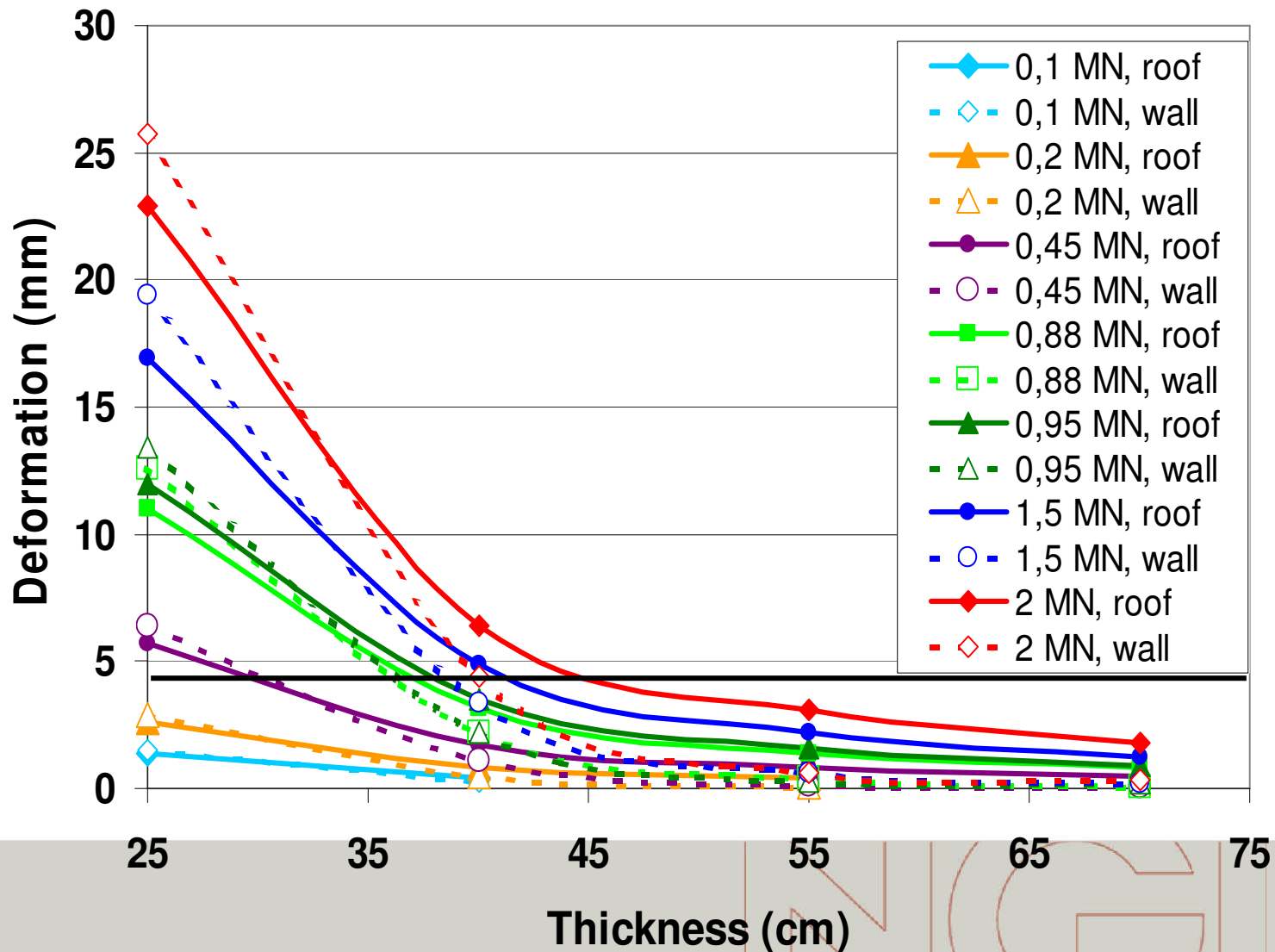
SEEN PERPENDICULAR TO THE TUNNEL AXIS



**Reinforced ribs of sprayed concrete in the 22 m wide National Theater Metro Station in Oslo, Norway. Used as the permanent support.**

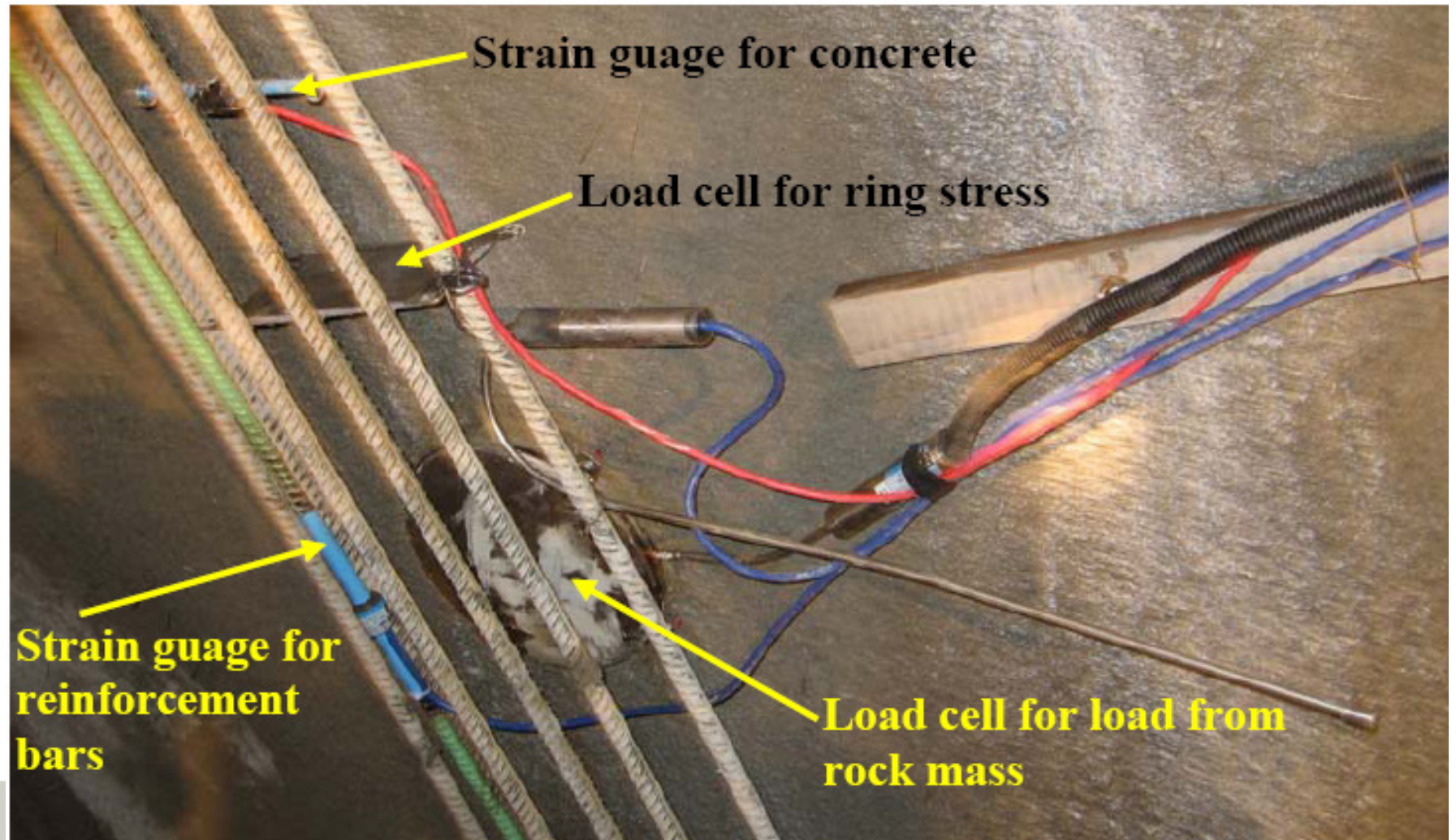


## Deformations in the crown and walls related to thickness of RRS and load in a 10 m wide tunnel

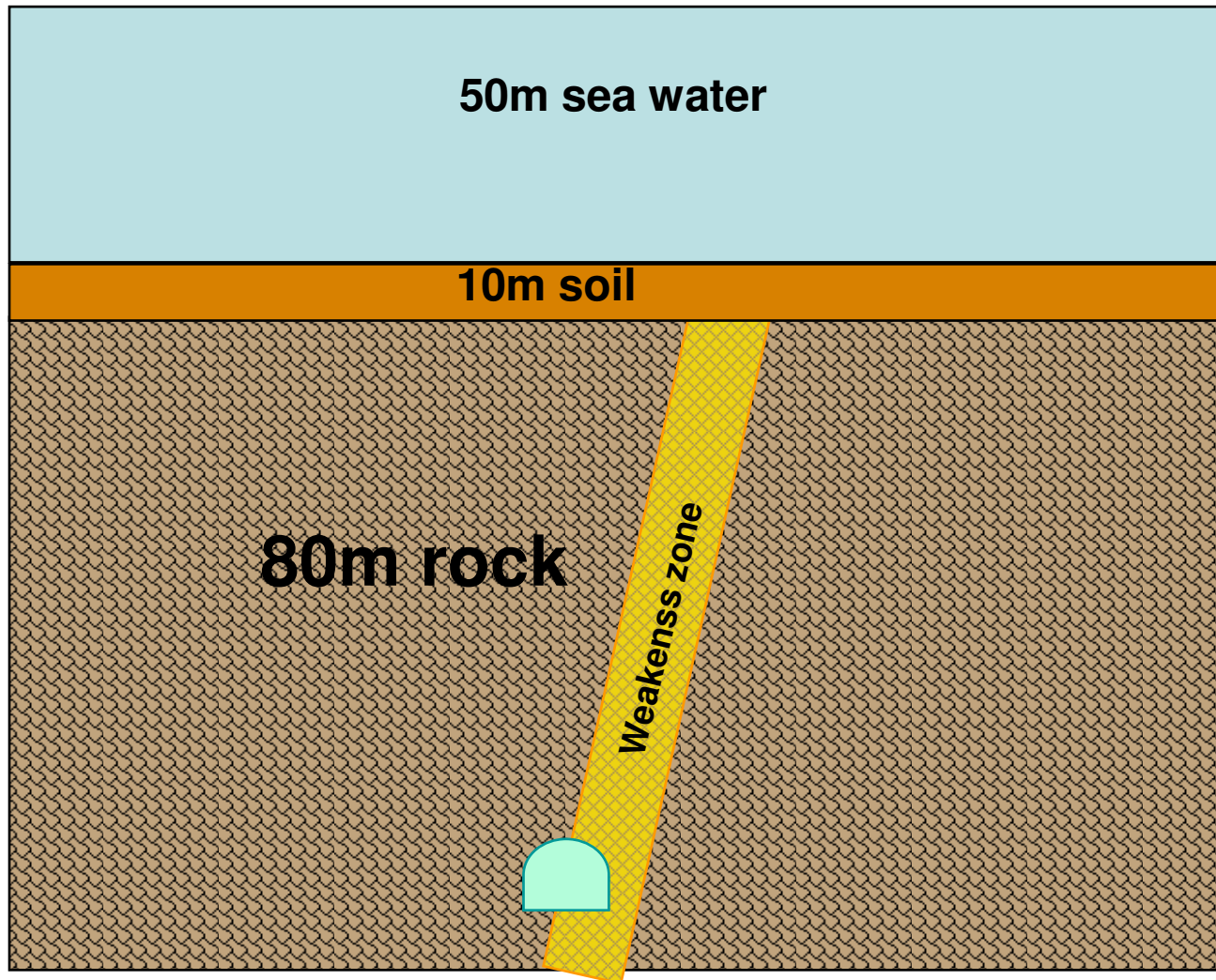




## Installment of instruments in a RRS



# Finnfast subesea tunnel

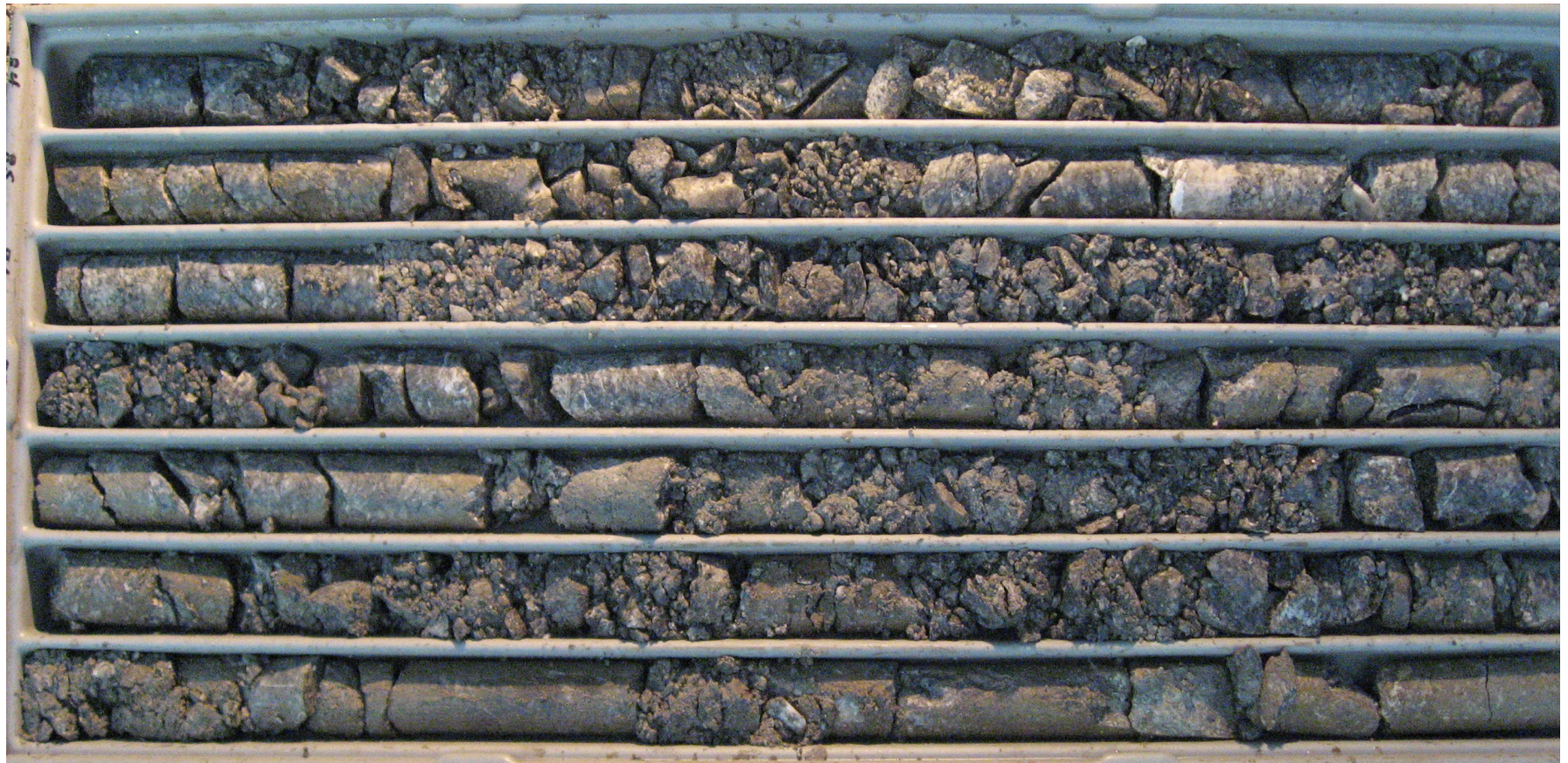




## Drill core from the instrumented weakness zone

Rock mass quality,  $Q = (10/20) \times (1/10) \times (1/5) = 0,01$

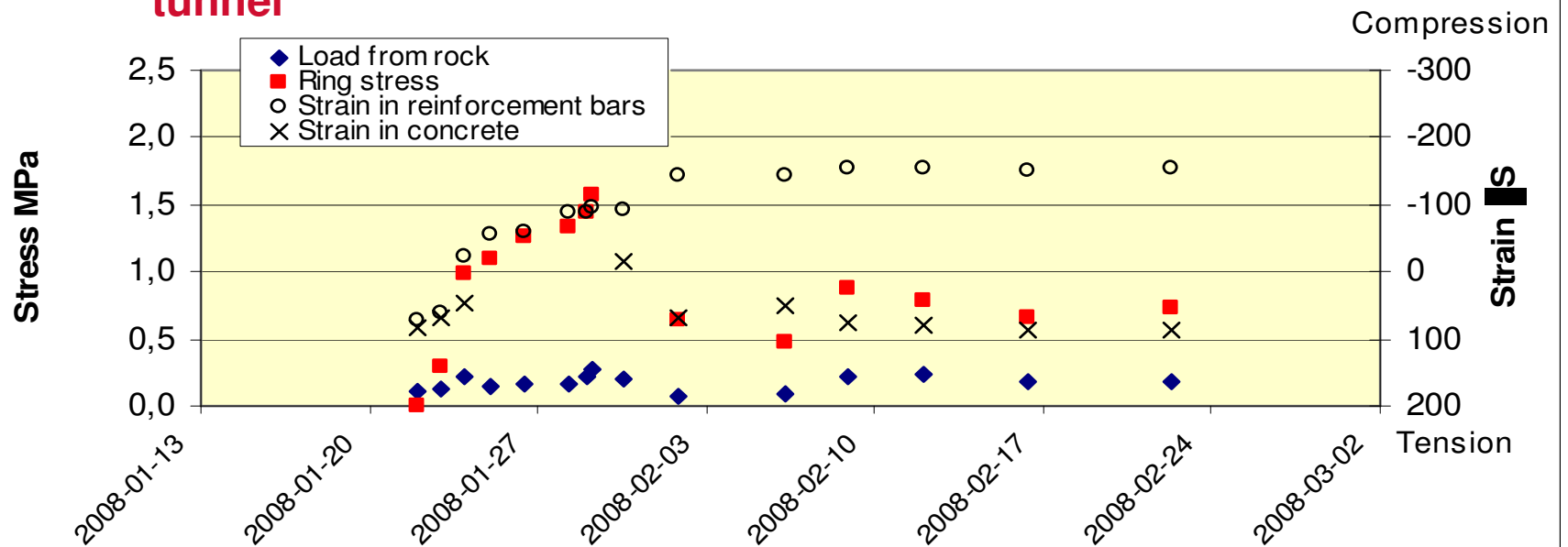
Exceptionally to Extremely poor. Contains swelling clay.



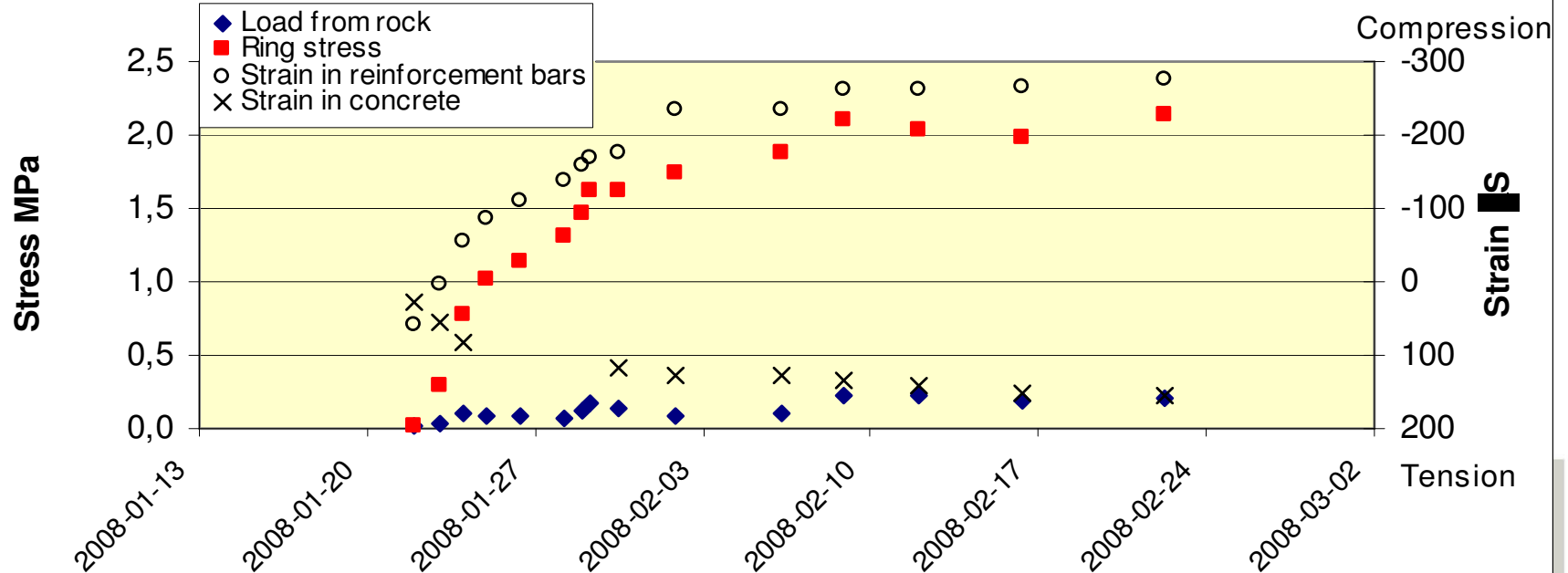


## Finnfast subsea tunnel

### Right hand springline



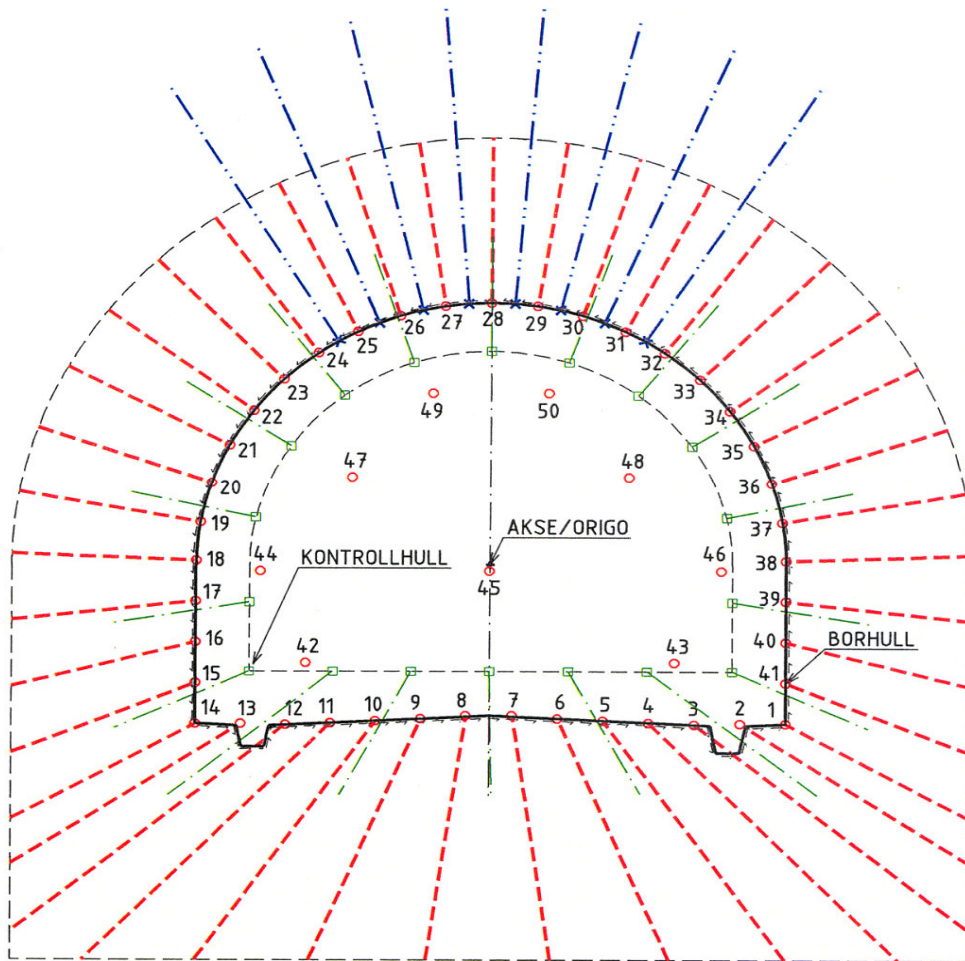
### Left hand spring line



# Conclusion

- The load from the rock seems to be lower than expected from theoretical calculation. This is most apparent in the crown.
- Both measurements and numerical simulation indicate tension in the rock close to the crown
- An even profile of the rib make it possible to calculate its capacity
- Strain measurements is more consistent than load cells
- Long term creep in the concrete stabilize after about two months
- Shrinkage in the concrete during curing ( $\approx 0,5-1,0 \text{ ‰} = 10-20\text{mm}$  in 20m rib length) may give tension in the contact between the rib and the crown

# Drill holes for pregrouting (50 holes)



TABELL OVER HULLANSETT, RETNING I FORHOLD TIL TUNNELAKSEN OG LENGDER.

HULL NR.		
PRIMÆSKJERM:	TUNNELAKSE	LENGDE
SÅLE:		
1, 2, 4, 5, 7, 8, 10, 11, 13, 14	11°	21 m
3, 6, 9, 12	25°	15 m
VEGG/HENG:		
16, 17, 19, 20, 22, 23, 25, 26, 28, 30, 31, 33, 34, 36, 37, 39, 40	10°	21 m
15, 18, 21, 24, 27, 29, 32, 35, 38, 41	23°	12 m
STUFF:		
42 - 50	0°	21 m
KONTROLLSKJERM ETTER INJEKSJON:		
SÅLE: 7 HULL	11°	15 m
VEGG/HENG: 11 HULL	10°	15 m
EKSTRAHULL VED OVERDEKNING MINDRE ENN 12-15 m:		
HENG: 8 HULL	20°	21 m

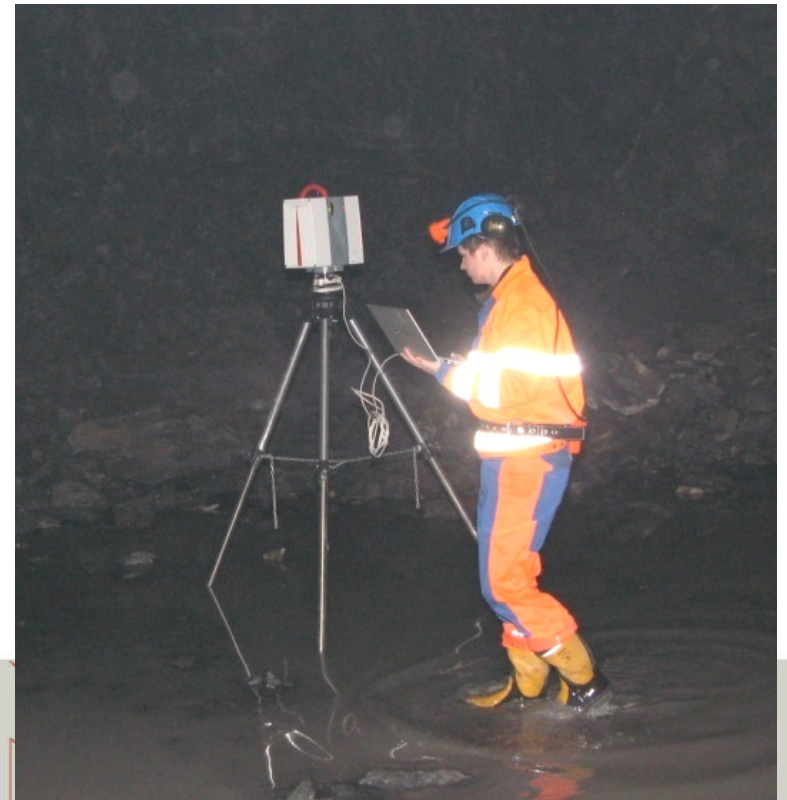
Cross section

## Data collection in tunnels under excavation



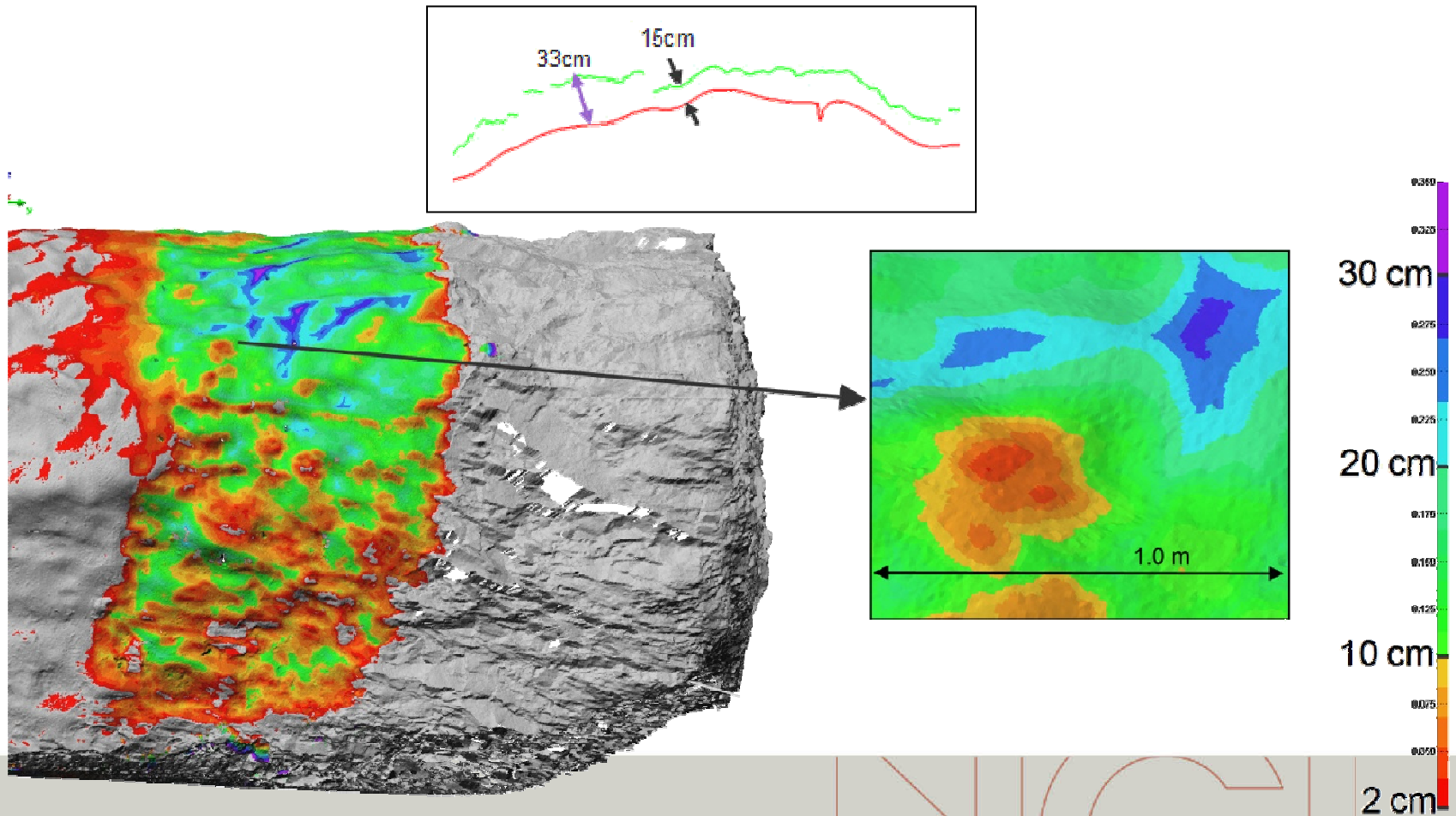
**Set-up, scan, pack up:  
8 minutes**

Leica HDS6000





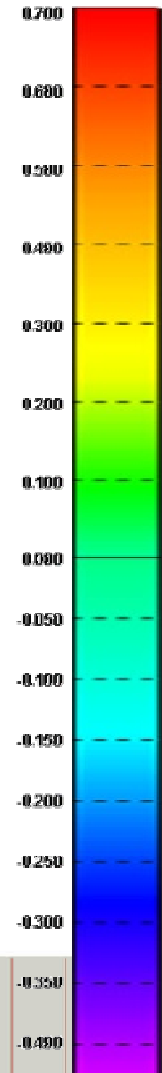
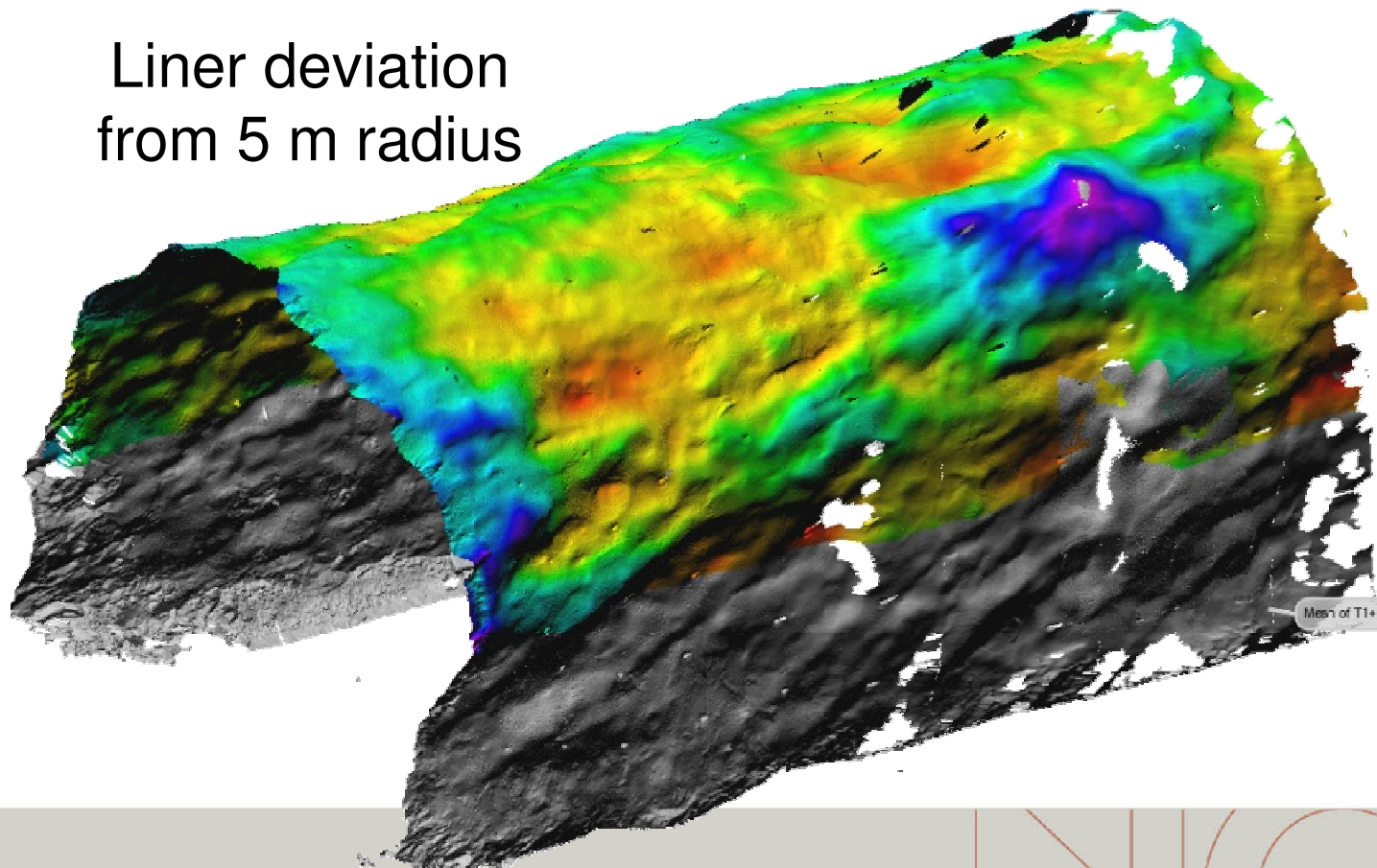
## Shotcrete Thickness Quality Control



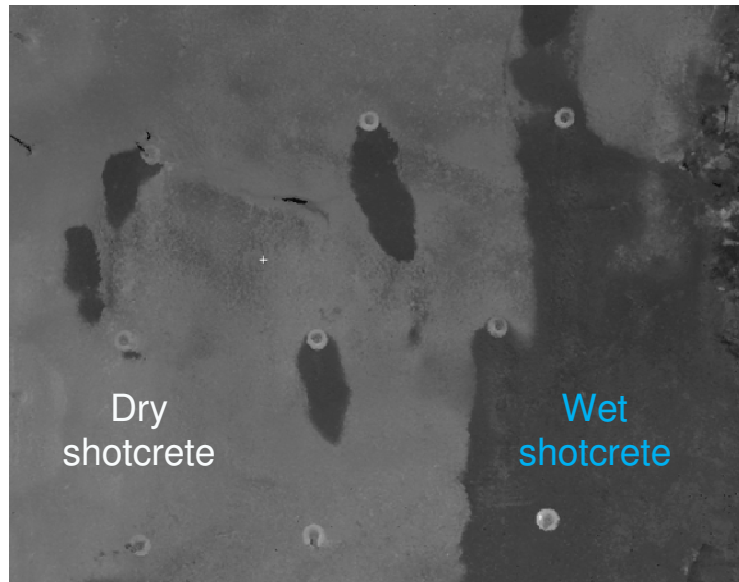
## Verifying as-built lined tunnel geometry



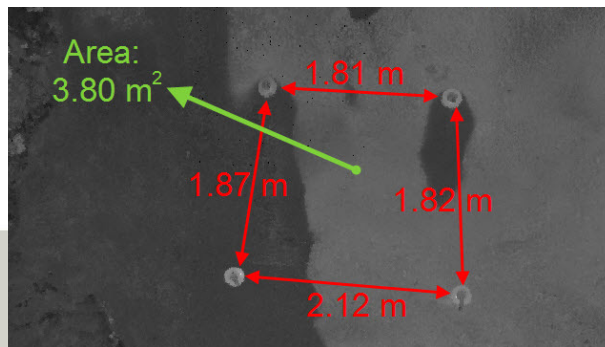
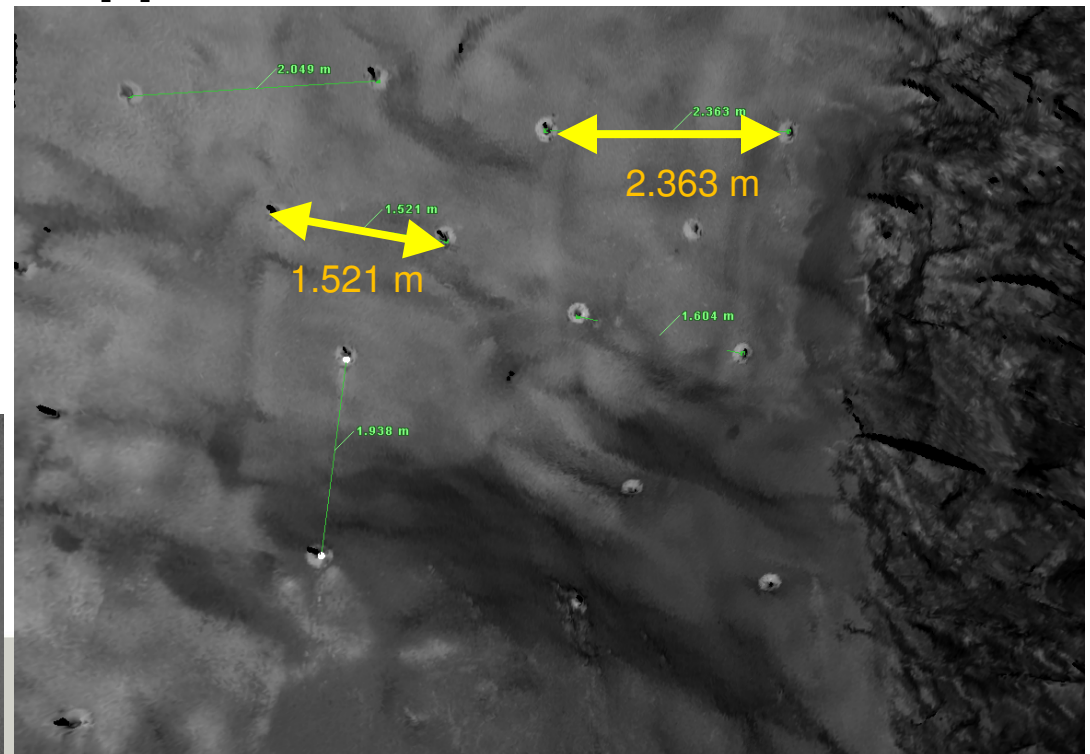
Liner deviation  
from 5 m radius



## Potential leakage zones

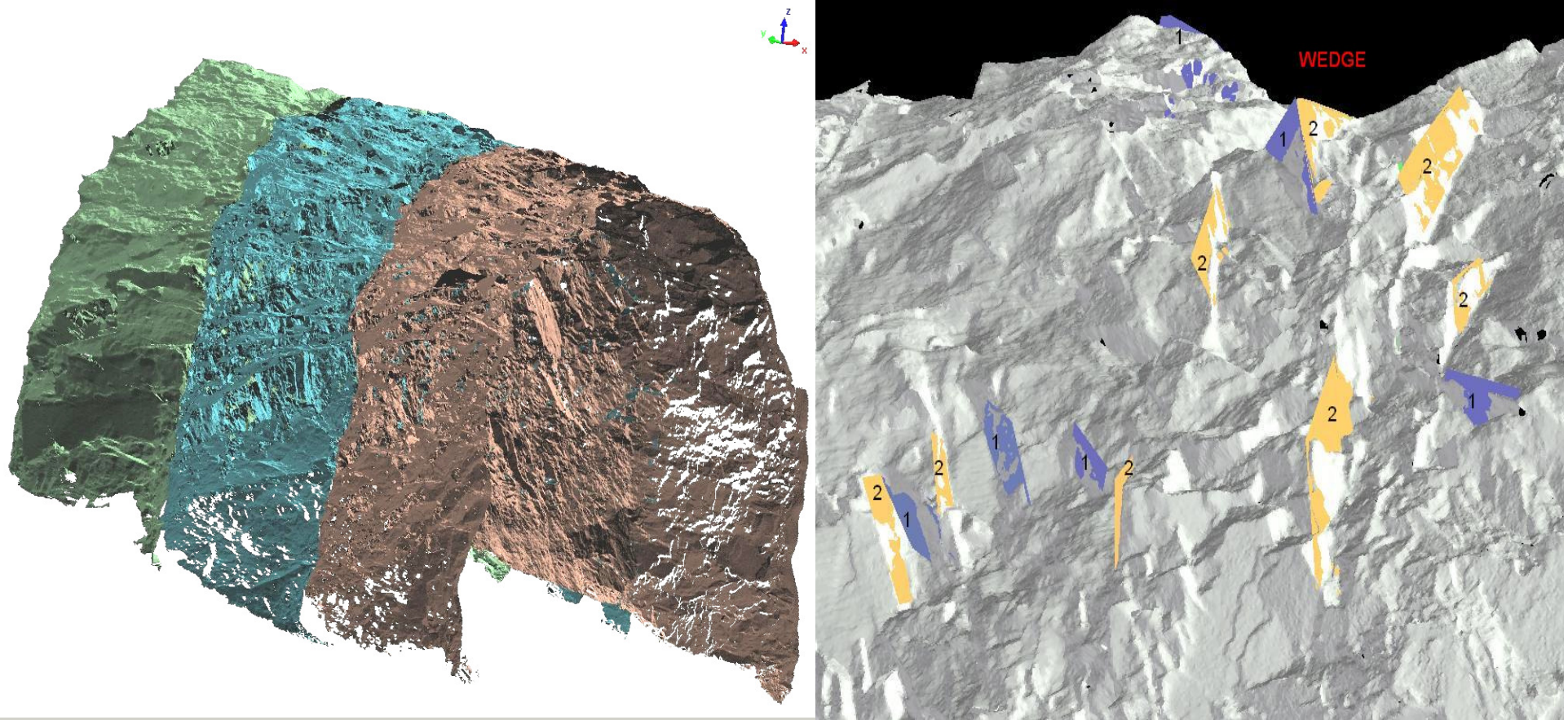


## Support installation

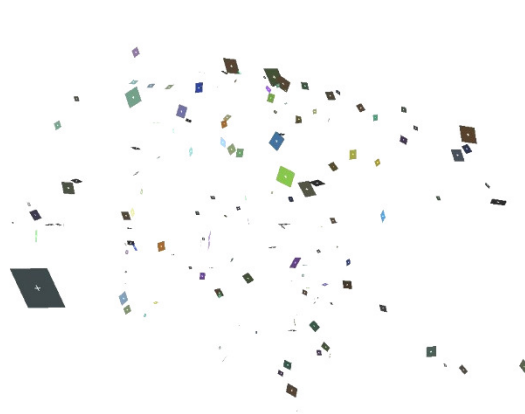
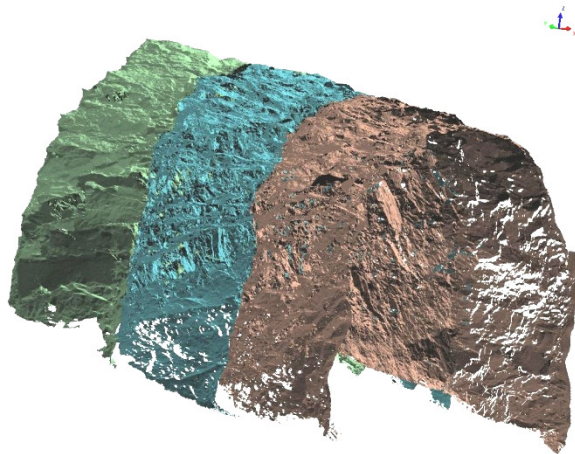




## Joint surfaces identified defining joint sets

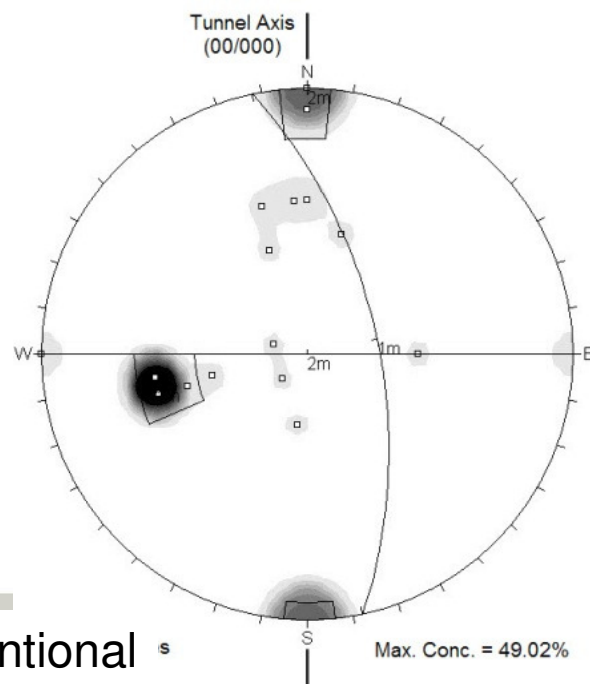




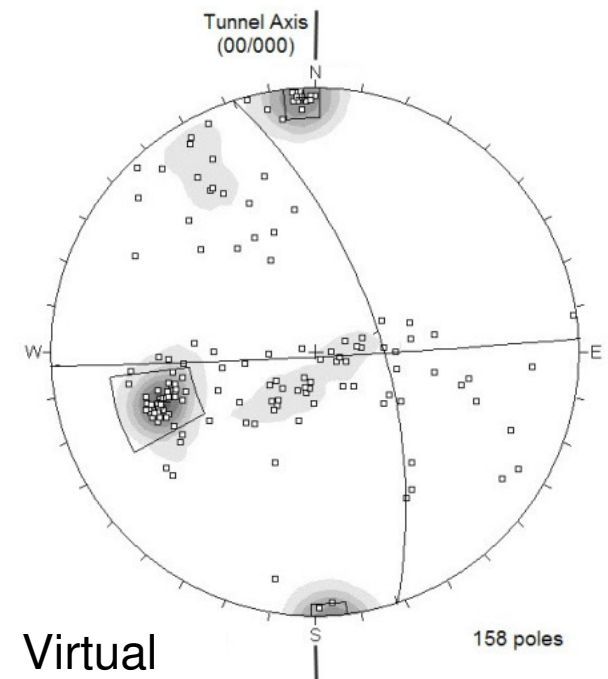
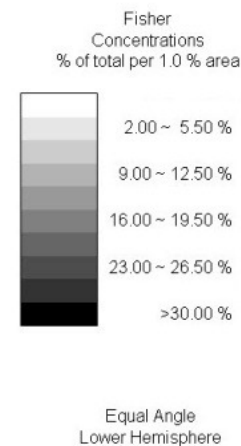


Joint  
surfaces  
identified

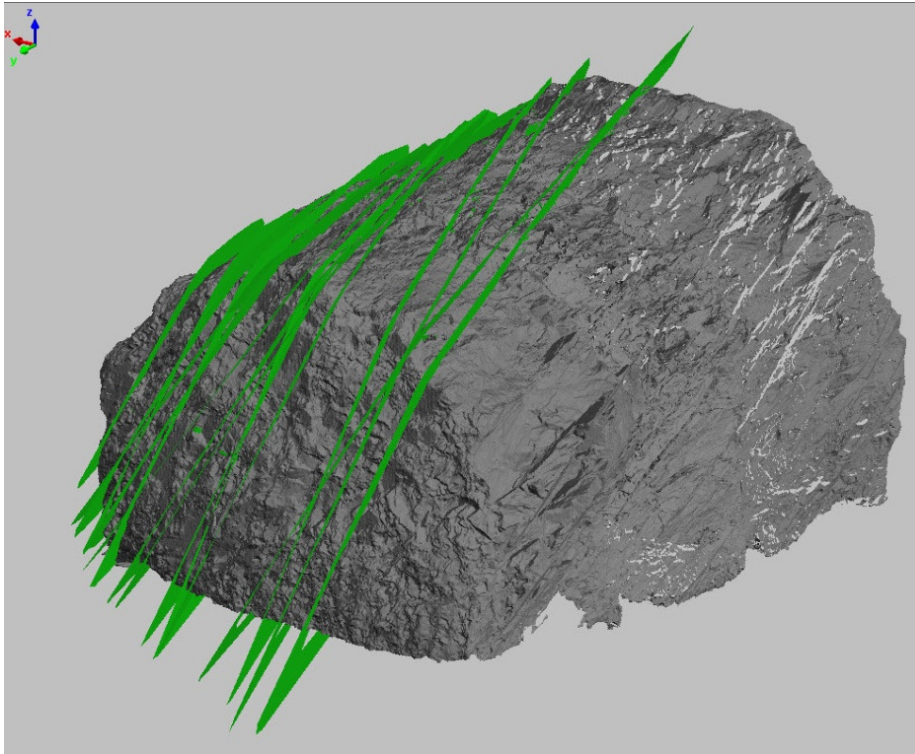
Three aligned 5  
m scans-  
rock surface only



Conventional  
mapping

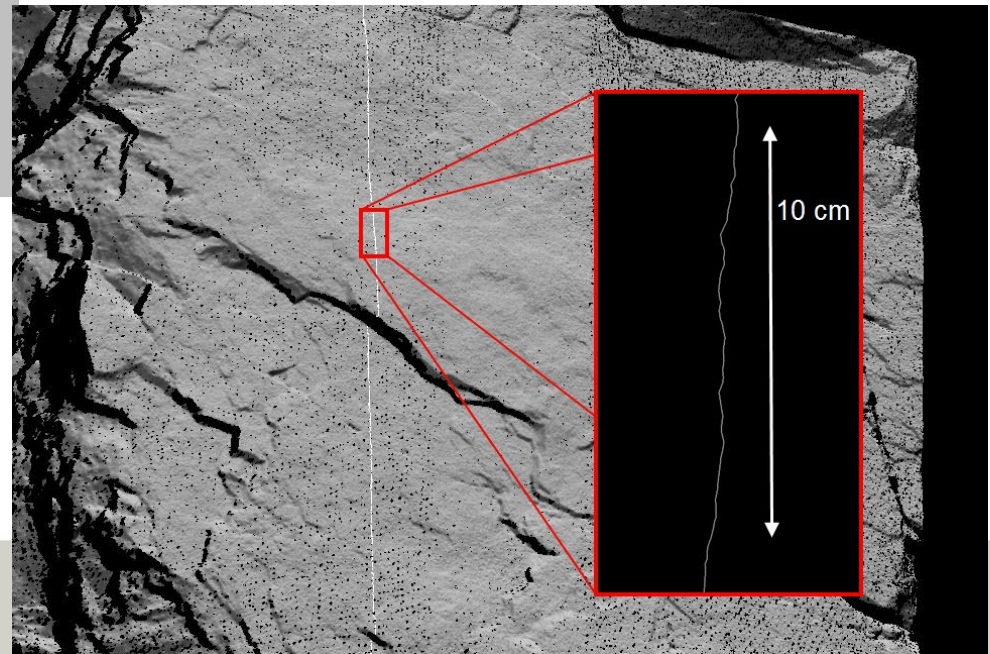


Virtual  
mapping

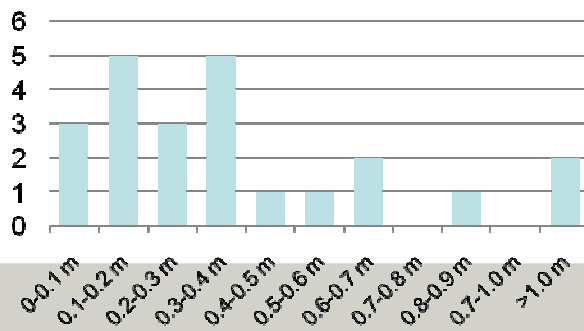


## Joint spacing and roughness

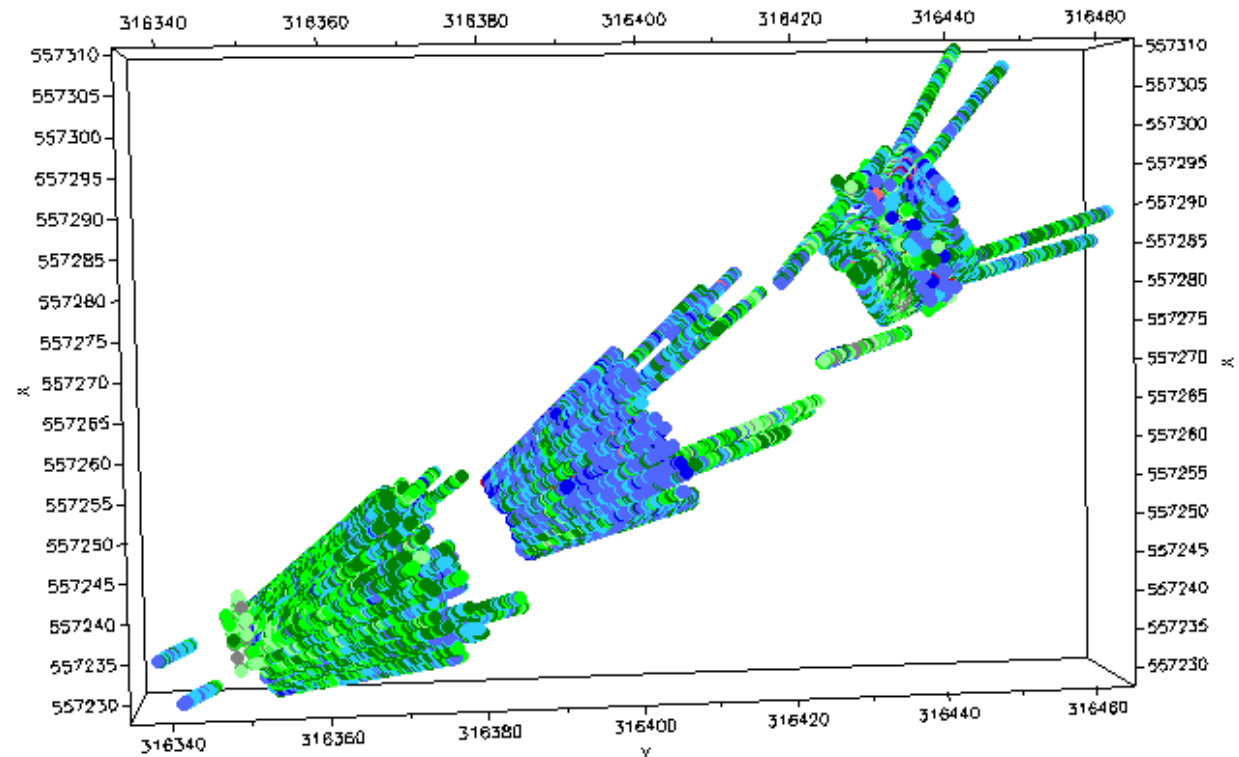
Roughness profile



Joint spacing distribution



# Measure while drilling



- Correlate 5 parameters from the drilling rig
- Gives data from all the drill holes, which may be correlated to Lidar data after blasting.

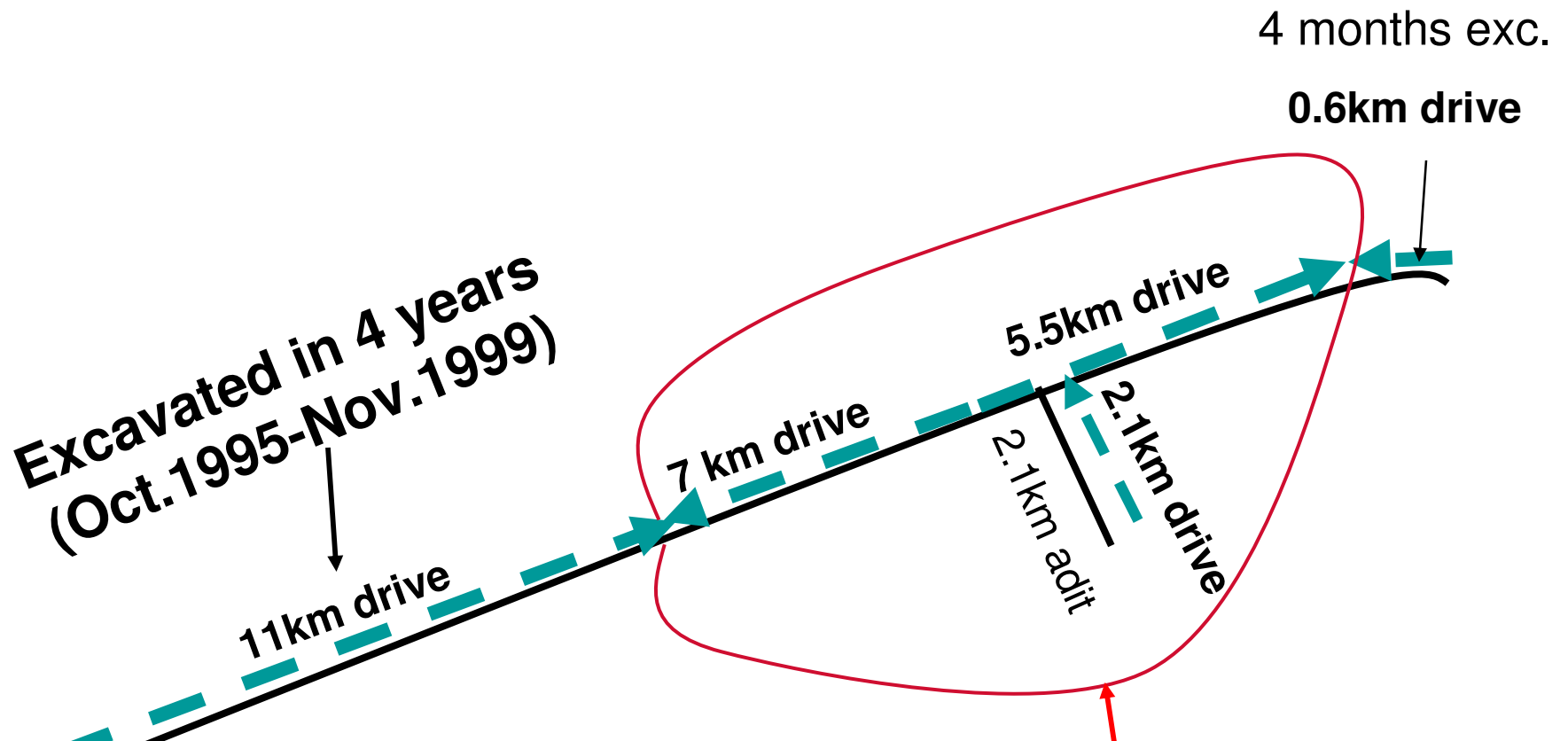
# The Lærdal Tunnel-

## The longest road tunnel of the world

- Length of the main tunnel 24.5km
- Access/ventilation tunnel 2.1km
- Cross section (theoretical) 56.5m<sup>2</sup>
- Overburden max. 1450m
- 20km more than 800m overburden
- 3 roundabouts (each 6km) span 31m
- 16 turning points (niches) span 12m
- Max. theoretical vertical stress = 39MPa. The major and dominant stress was subhorizontal



# The 24.5 km long Lærdal road Tunnel



**Sum 14.6km Excavated in 3.5 years. (April 1996-Nov.1999)**

**Max. excavation per week per face was 108 m.**

# Total cost for the Lærdal tunnel when opened for traffic in the year 2000

- 1050 mill NOK  $\approx$  120 mill Euro  $\approx$  230 mill SGD
- 39300 NOK  $\approx$  4400 Euro  $\approx$  8700 SGD per meter tunnel
- 26700m excavated and supported, included access tunnel
- Included ventilation and illumination
- Included drainage system
- Included water shielding and frost protection (Rel. dry tunnel)
- Included warning and security measures
- Included 100m bypass tunnel for gas and dust cleaning

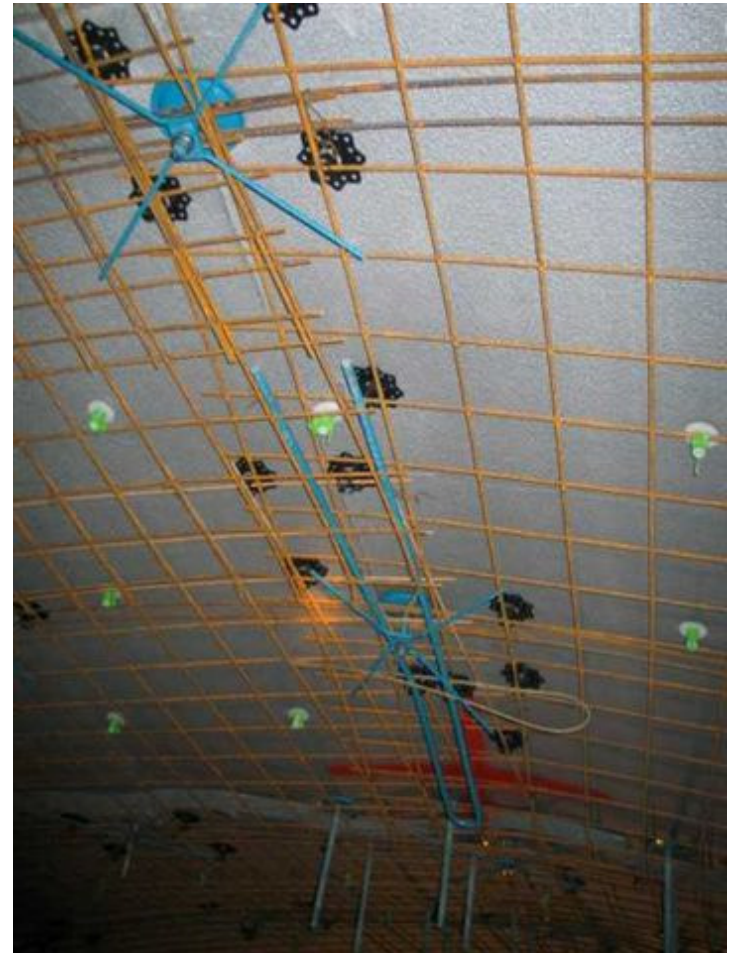
## Poor rock mass quality gives deformation

- Empirical relation between deformation and rock mass quality,  $Q$
- The temporary support will be deformed in poor rock
- Need for high residual strength and energy absorption in  $S_{fr} + B$  in poor rock
- Early installation of rigid support gives cracking and some times collapse in high stress or squeezing rock
- Installation of more rigid support when the deformation has been reduced to an accepted level
- During the last 15-20 years RRS has replaced CCA in the lowest rock mass qualities in Norway

# Water and frost protection

PE-foam and mesh reinforced shotcrete.

Micro polypropylene fiber in shotcrete as fire protection



Precast elements in the wall



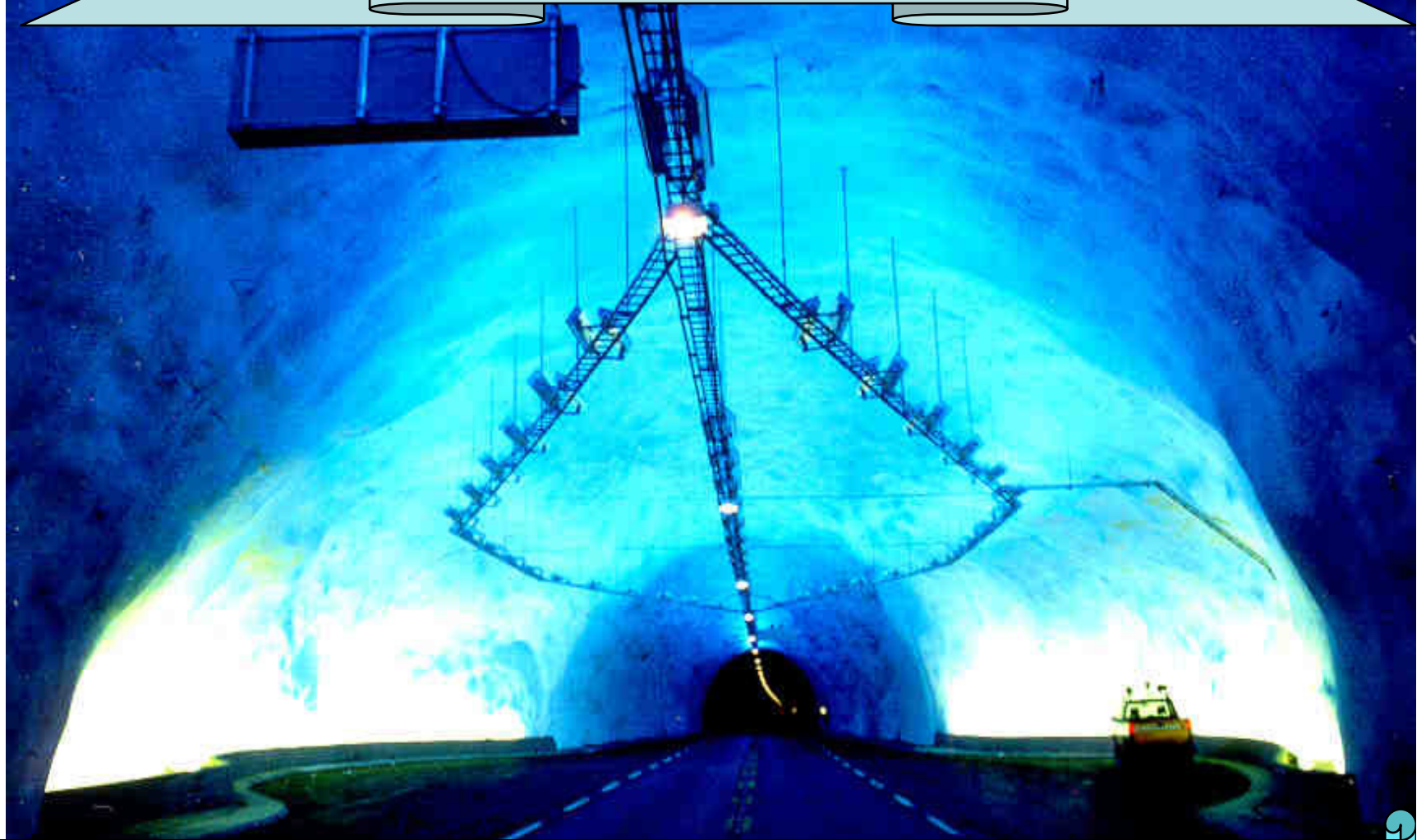


## Water and frost insulation. Precast segments in the walls



NGI

*Thank you*



31M WIDE TURNAROUND CAVERNS IN THE  
24,5KM LONG LÆRDAL ROAD TUNNEL